

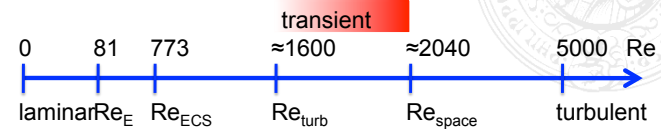
Turbulence – and related problems

- Lecture 1: Transition: Coherent structures
- Lecture 2: Transition: Transient turbulence
- Lecture 3: Global transport

Bruno Eckhardt

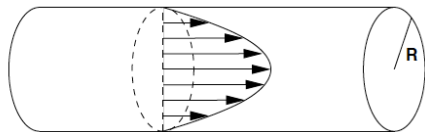


Reynolds numbers for pipe flow (not to scale)



- Re_E Energy stability
- Re_{ECS} Coherent structures appear
- Re_{turb} Turbulence appears in experiments
- Re_{space} Turbulence becomes spacefilling

Pipe flow



- Laminar: Hagen-Poiseuille law

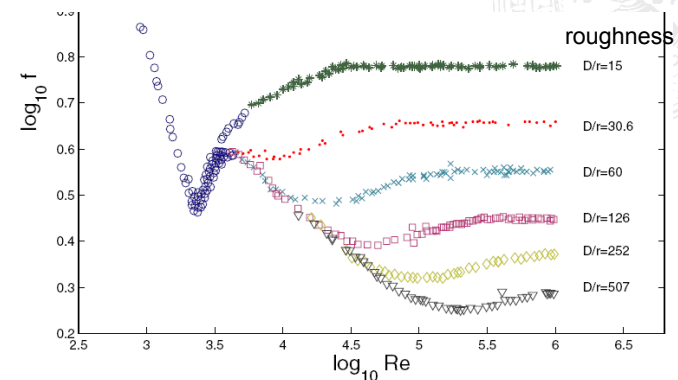
volume flow

$$Q = \frac{\pi}{8\eta} \frac{\Delta p}{L} R^4$$

- Turbulent: Friction law

$$\frac{\Delta p}{\rho L} = f \frac{U^2}{4R}$$

Nikuradse 1932/1933



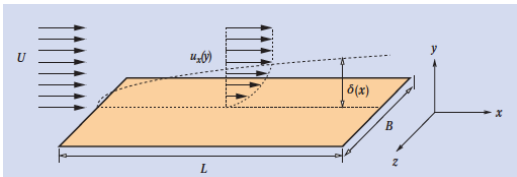
from Goldenfeld, PRL **96**, 044503 (2006)

Mean profiles: Blasius

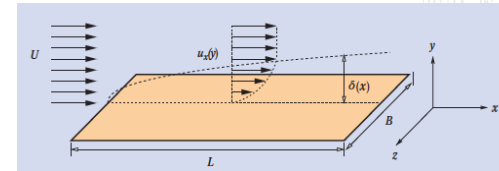
$$\cancel{\partial_x u_x} + \partial_x(u_x u_x) + \partial_y(u_y u_x) + \partial_z(\cancel{u_z u_x}) = -\partial_x p + \nu(\cancel{\partial_{xx} u_x} + \partial_{yy} u_x + \cancel{\partial_{zz} u_x})$$

$$\partial_x(u_x u_x) + \partial_y(u_y u_x) = -\partial_x p + \nu \partial_{yy} u_x$$

$$\partial_x u_x + \partial_y u_y = 0$$



Prandtl 1904:



$$\delta(x) = \sqrt{x\nu/U}$$

Local force proportional to

- free stream velocity
- 1/boundary layer thickness
- width . dx

$$dF \propto \rho \nu \cdot \frac{U}{\delta(x)} \cdot B dx$$

$$F \propto 1,1 \rho B L U^2 / \sqrt{Re}$$

$$Re = LU/\nu$$

Mean profiles: Prandtl-von Karman

$$\cancel{\partial_x u_x} + \partial_x(\cancel{u_x u_x}) + \partial_y(u_y u_x) + \partial_z(\cancel{u_z u_x}) = -\partial_x p + \nu(\cancel{\partial_{xx} u_x} + \partial_{yy} u_x + \cancel{\partial_{zz} u_x})$$

$$\partial_y(\langle u'_y u'_x \rangle) - \nu \partial_y u_x = 0$$

Momentum balance

Mixing length model $\langle u'_y u'_x \rangle = -l^2 (\partial_y u_x)^2$

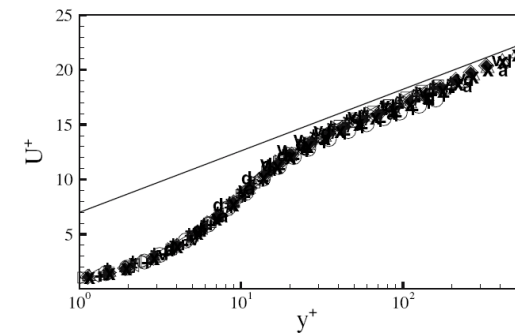
$$l = \kappa y$$

$$u_x = A \ln y + B$$

Law of the wall

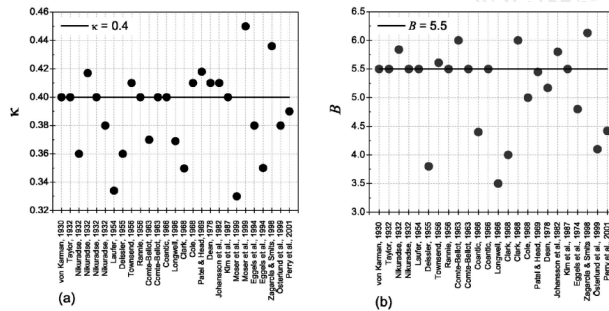
Turbulent boundary layer

$$U^+ = \frac{1}{\kappa} \ln y^+ + B$$



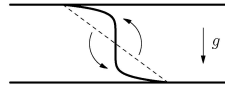
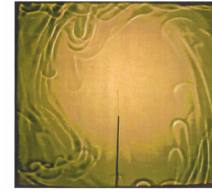
Law of the wall

$$U^+ = \frac{1}{\kappa} \ln y^+ + B$$

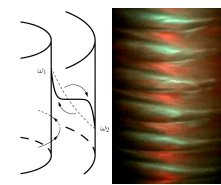


Zanoun+Durst+Naghib, Phys Fluids 15 (2003) 3079

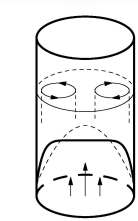
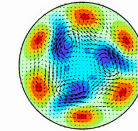
Rayleigh-Benard



Taylor-Couette

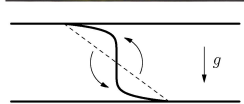
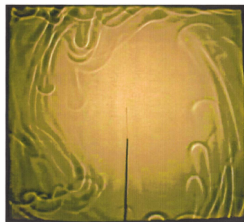


Pipe flow



Obs: External forcing induces transverse velocity fluctuations
Q: what can one say about the global scaling?

The Rayleigh-Bénard problem



Input:	Temp. Diff.	Rayleigh number	Ra
	Material	Prandtl number	Pr
Output:	„Wind“	Reynolds number	Re
	Heat flux	Nusselt number	Nu

Wanted:
the response of the fluid

$$Re(Ra, Pr) \approx Ra^\alpha Pr^\beta$$

$$Nu(Ra, Pr) \approx Ra^\gamma Pr^\delta$$

Nu(Ra)

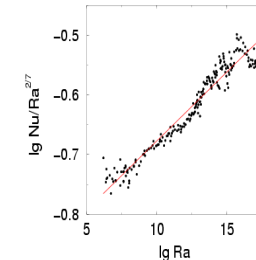
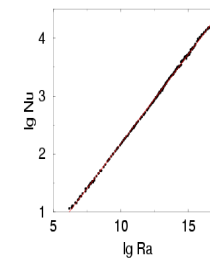
data:
cryogenic helium
approximate
power laws only

$$Nu \sim Ra^\beta$$

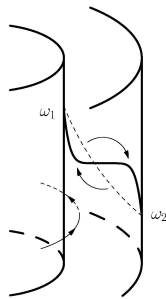
$$\beta = 2/7 \approx 0.286 \quad (\text{Castaing et al., JFM 204, 1 (1989), Siggia, ARFM. 26, 137 (1994)})$$

$$\beta \approx 0.309 \quad (\text{Niemela et al., Nature 404, 837 (2000)})$$

exponent varies
with Ra: $\beta(Ra)$



The Taylor-Couette problem



Fluid between independently rotating cylinders

Input:	Rotation rates	Reynolds numbers Re_{inner}, Re_{outer}
	Geometry	„Prandtl number“ Pr
Output:	„Wind“	Reynolds number Re_w
	Angular momentum flux	Nusselt number Nu

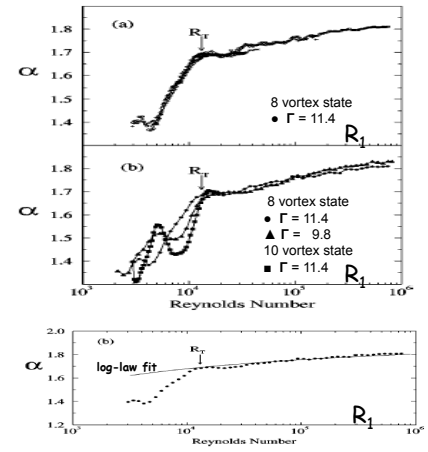
Wanted:

(Outer cylinder at rest)

$$Re_w(Re_{inner}, Pr) \approx Re_{inner}^\alpha Pr^\beta$$

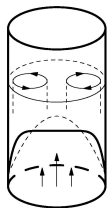
$$Nu_\omega(Re_{inner}, Pr) \approx Re_{inner}^\gamma Pr^\delta$$

Local exponents $\alpha(R_1)$ in $G \sim R_1^\alpha$



Lewis Swinney PRE59 5457(1999)

Pipe flow



Pressure driven flow down a circular pipe

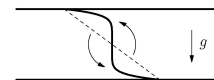
Input:	Mean flux	Re
Output:	„Wind“	Reynolds number Re_w
	Momentum flux	Nusselt number Nu_z

Wanted:

$$Re_w(Re)$$

$$Nu_z(Re)$$

Rayleigh-Bénard



Heat transport enhanced by flow

Transport measured by Nusselt number:

$$Nu = \langle u_z \theta \rangle_{x,y,t} - \nu \partial_z \langle \theta \rangle_{x,y,t}$$

Energy dissipation in velocity field

$$\varepsilon = Pr^{-2} Ra(Nu-1)$$

$$Pr = \nu / \kappa$$

Taylor-Couette



Transport of angular velocity

Dimensionless Nusselt number

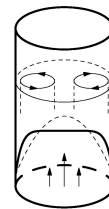
$$Nu_\omega = r^3 \left(\langle u_r \omega \rangle - \nu \partial_r \langle \omega \rangle \right)$$

Energy dissipation in excess of laminar dissipation:

$$\varepsilon = \varepsilon_{tot} - \varepsilon_{lam} = \sigma^{-2} Ta (Nu_\omega - 1)$$

$$\sigma = \left(\frac{(1+\eta)\sqrt{2}}{\sqrt{\eta}} \right)^4 \quad \text{„Prandtl number“}$$

Pipe flow



Transport of momentum

Dimensionless Nusselt number

$$Nu_z = r^{-1} \left(\langle u_r u_z \rangle - \nu \partial_z \langle u_z \rangle \right)$$

Energy dissipation in excess of laminar dissipation:

$$\varepsilon = \varepsilon_{tot} - \varepsilon_{lam} = Re^2 (Nu_\omega - 1)$$

Analogies

Transport

Dissipation

RB $Nu = \langle u_z \theta \rangle_{x,y,t} - \nu \partial_z \langle \theta \rangle_{x,y,t}$ $\varepsilon = Pr^{-2} Ra (Nu - 1)$

TC $Nu_\omega = r^3 \left(\langle u_r \omega \rangle - \nu \partial_r \langle \omega \rangle \right)$ $\varepsilon = \sigma^{-2} Ta (Nu_\omega - 1)$

Pipe $Nu_z = r^{-1} \left(\langle u_r u_z \rangle - \nu \partial_z \langle u_z \rangle \right)$ $\varepsilon = Re^2 (Nu_\omega - 1)$

Rayleigh-Bénard (I)

Two equations:

$$\varepsilon = Pr^{-2} Ra (Nu - 1) \quad \lambda \propto 1 / Nu \quad \text{thermal BL}$$

$$Nu = \langle u_z \theta \rangle_{x,y,t} - \kappa \partial_z \langle \theta \rangle_{x,y,t} \quad \delta \propto 1 / \sqrt{Re} \quad \text{velocity BL}$$

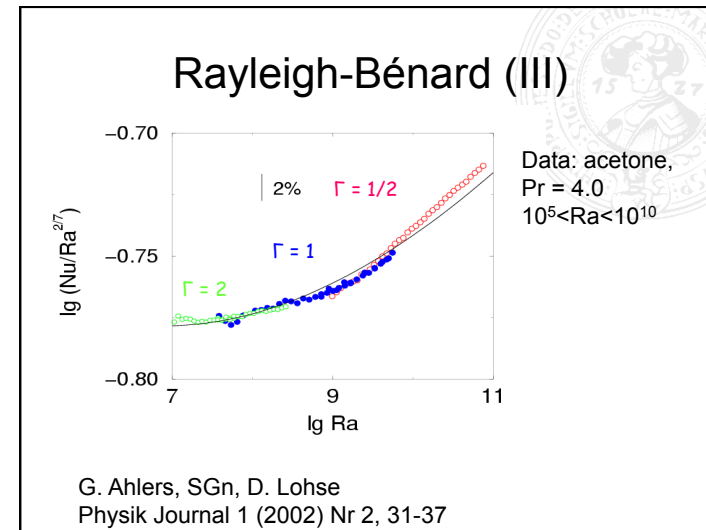
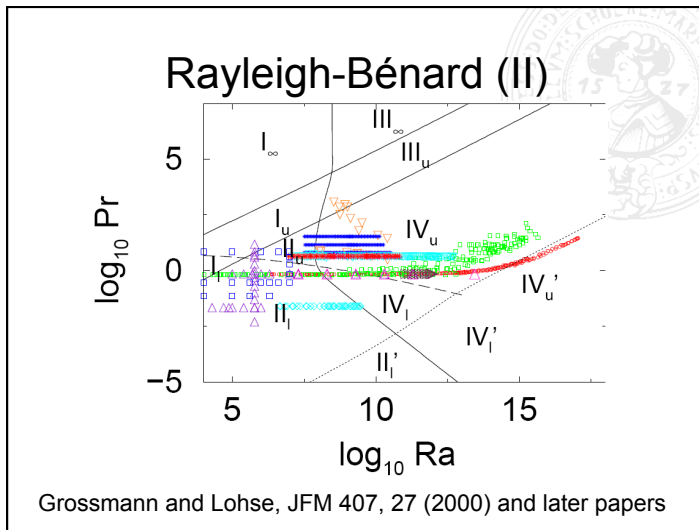
Two models:

$$\varepsilon = Pr^{-2} Ra Nu = c_2 Re^3 + c_1 Re^{5/2}$$

$$Nu = c_4 Re Pr f(\lambda / \delta) + c_3 \sqrt{Re Pr} f(\lambda / \delta)$$

$$f(\lambda / \delta) \text{ switches between } 1 \quad \lambda > \delta$$

$$\text{and } \lambda / \delta \text{ for } \lambda < \delta$$



Taylor-Couette

Two equations: TC RB

$$\varepsilon = \sigma^{-2} Ta (Nu_w - 1) \quad \varepsilon = Pr^{-2} Ra (Nu - 1)$$

$$Nu_w = r^3 \left(\langle u_r \omega \rangle - \nu \partial_r \langle \omega \rangle \right) \quad Nu = \langle u_z \theta \rangle_{x,y,t} - \nu \partial_z \langle \theta \rangle_{x,y,t}$$

Two models: „Prandtl number:“

$$\varepsilon = c_2 Re_w^3 + c_1 Re_w^{5/2} \quad \sigma = \left(\frac{(1+\eta)/\sqrt{2}}{\sqrt{\eta}} \right)^4$$

$$Nu_w / \sigma = c_4 Re_w g(s) + c_3 \sqrt{Re_w g(s)} \quad s = \frac{\lambda}{\delta} = \frac{1}{2a} \frac{\sqrt{Re_w}}{Nu_w}$$

Predictions

Modelling transport and excess dissipation

All quantities determined by transverse velocity field: „wind“

Reynolds number Re_w

Energy dissipation

$$\varepsilon = c_2 Re_w^3 + c_1 Re_w^{5/2}$$

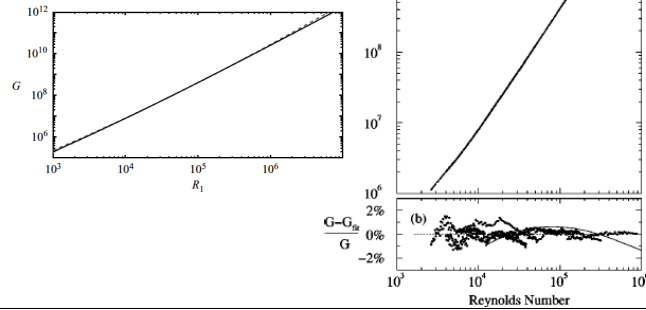
Momentum transport

$$Nu_w / \sigma = c_4 Re_w g(s) + c_3 \sqrt{Re_w g(s)} \quad s = \frac{\lambda}{\delta} = \frac{1}{2a} \frac{\sqrt{Re_w}}{Nu_w}$$

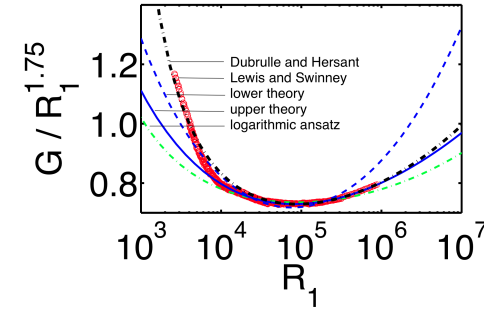
Fit coefficients and compare

Comparison to data

Lewis and Swinney,
PRE 59, 5457 (1999)



Taylor-Couette



Data: Lewis and Swinney, PRE 59, 5457 (1999)

Pipe flow

Two equations: Pipe

$$\varepsilon = \text{Re}^2 (Nu_w - 1)$$

$$Nu_w = r^{-1} \langle u_r u_z \rangle - \nu \partial_z \langle u_z \rangle$$

Two models:

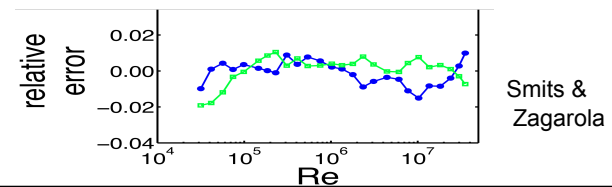
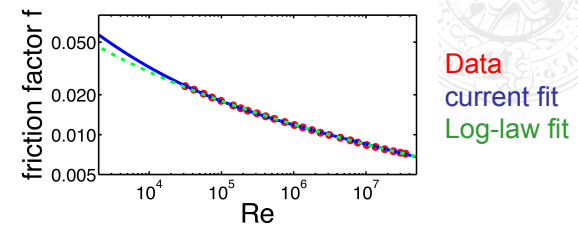
$$\varepsilon = c_2 \text{Re}_w^3 + c_1 \text{Re}_w^{5/2}$$

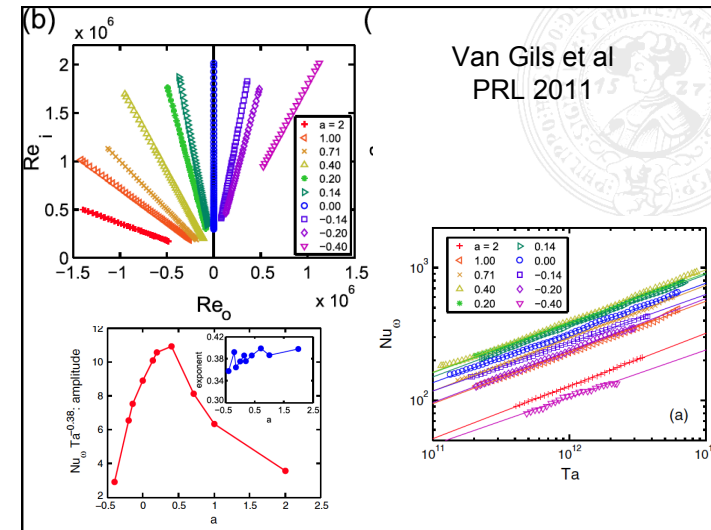
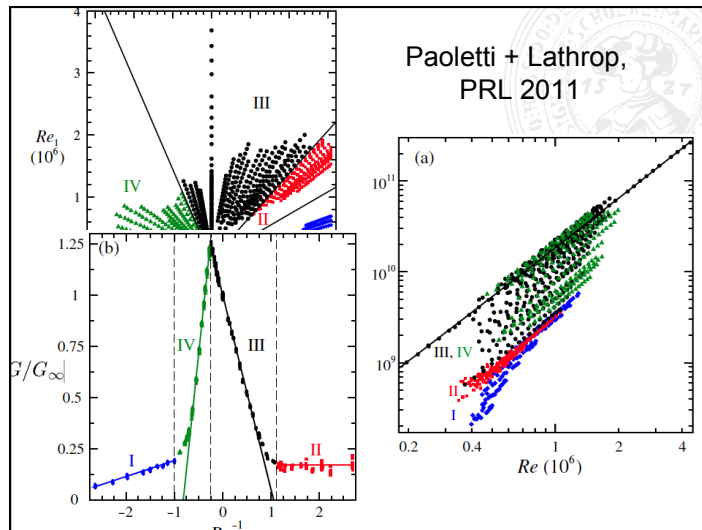
$$Nu_w = c_4 \text{Re}_w g(s) + c_3 \sqrt{\text{Re}_w} g(s)$$

$$s = \frac{\lambda}{\delta} = \frac{1}{2a} \sqrt{\text{Re}_w}$$

Predictions

Comparison to data





Conclusions:

- Analogy between RB, TC and pipe clarified
- Corresponding currents and wind dissipation identified
- Analogous modelling assumptions successfully tested
- To do: Analysis of most recent data