

The background features a 3x3 grid of circular droplets. Each droplet is surrounded by a thin, dark ring. In the top-left corner, there is a scale bar labeled '2 μm'. In the top-middle corner, there is a scale bar labeled '5 μm'. In the top-right corner, there is a scale bar labeled '15 μm'. A large, faint watermark 'Eric R Dufresne 2015' is oriented diagonally across the entire image.

Surface Tension, Droplets, and  
Contact Lines  
*Lecture III*

**Eric Dufresne**  
*Yale*

*Boulder Condensed Matter Summer School 2015*



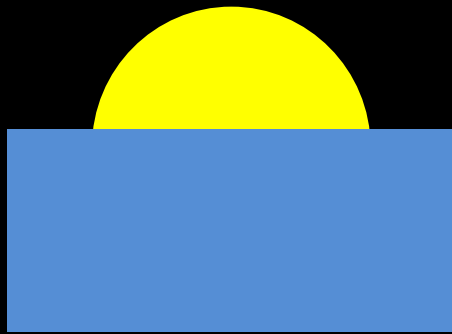
Dr. Rob Style

->Oxford

Elizabeth Jerison, Kate Jensen, Ye Xu, Ross Boltyanskiy, Larry  
Wilens, John Wettlaufer

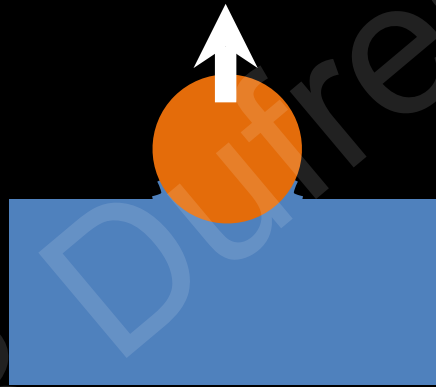
# Three Foundational Theories of Interfacial Mechanics

*Young-Dupre (18XX)*



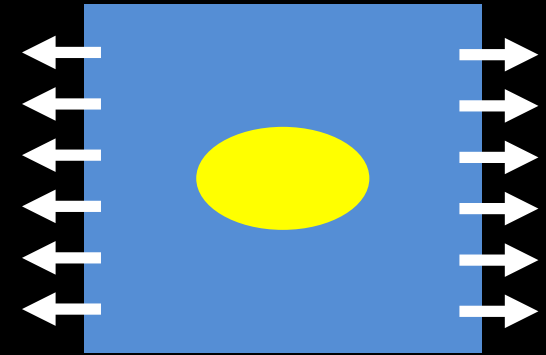
wetting

*JKR (1971)*



adhesion

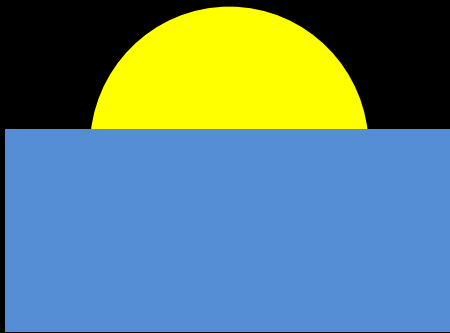
*Eshelby (1957)*



composites,  
fracture,  
dislocations

# Three Foundational Theories of Interfacial Mechanics

*Young-Dupre (18XX)*



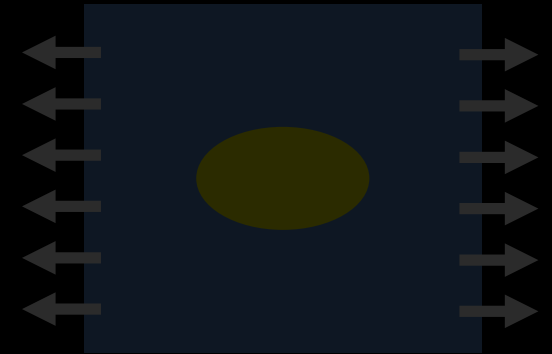
wetting

*JKR (1971)*



adhesion

*Eshelby (1957)*



composites,  
fracture,  
dislocations

3 kPa silicone gel ( 50  $\mu\text{m}$ )

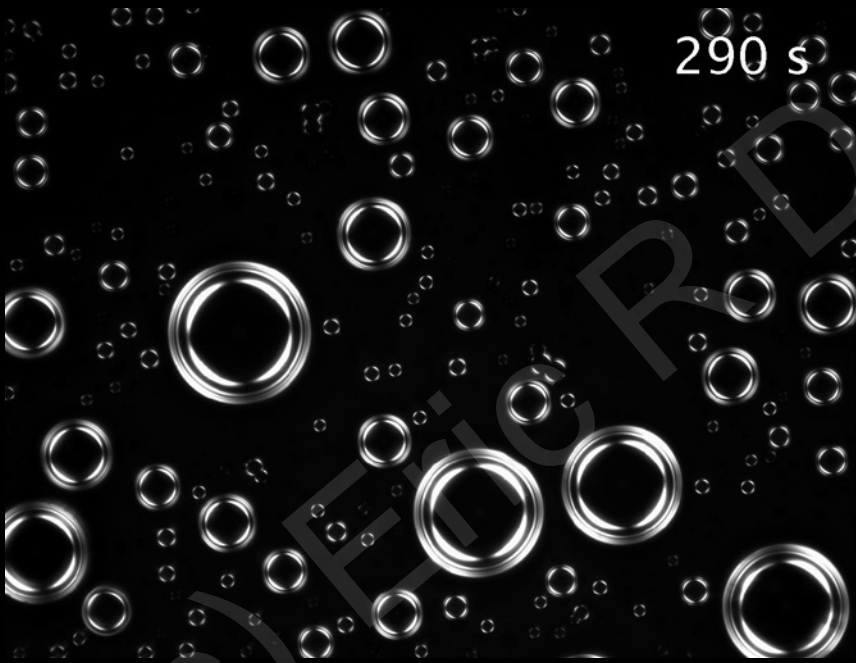
glass (coverslip)

1.8 MPa silicone elastomer ( 50  $\mu\text{m}$ )

glass (coverslip)

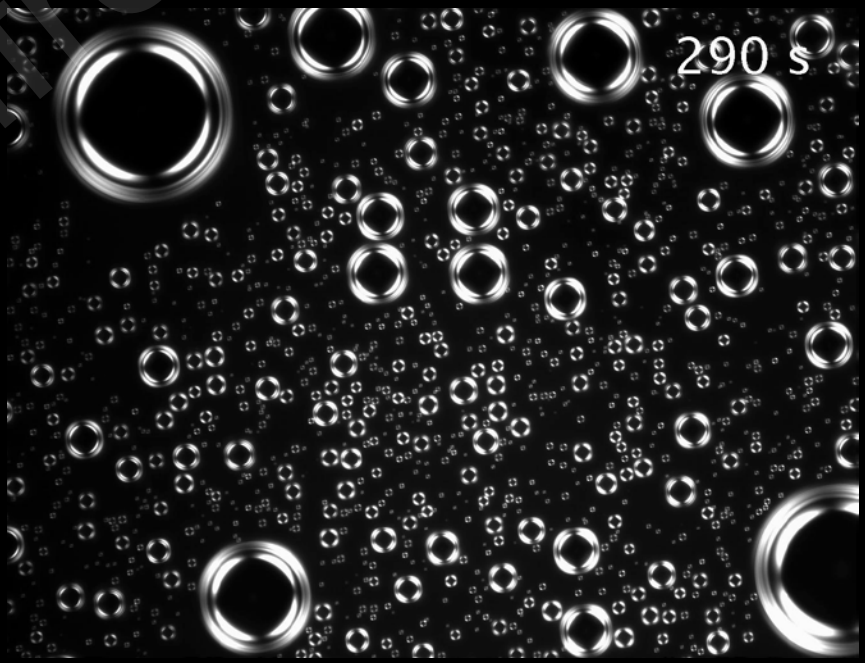
atomized glycerol

0.3mm

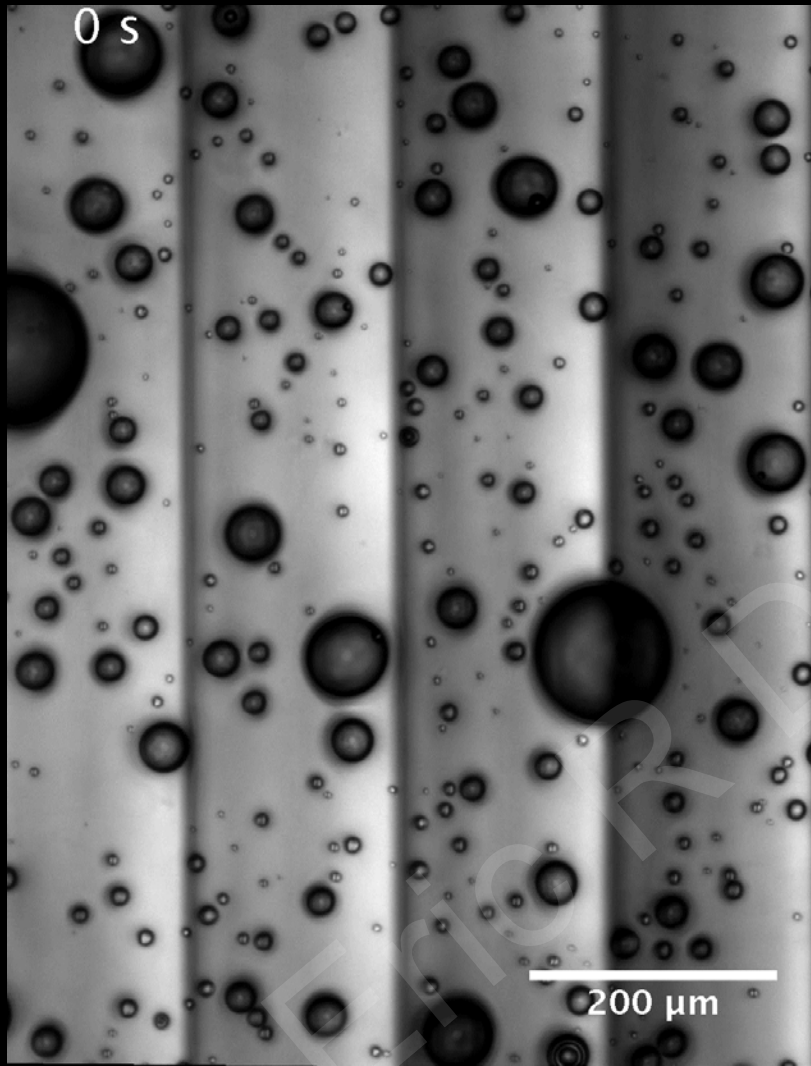


290 s

0.3mm



290 s



Atomized spray of glycerol  
on a flat surface of a  
soft substrate with a  
thickness/stiffness gradient



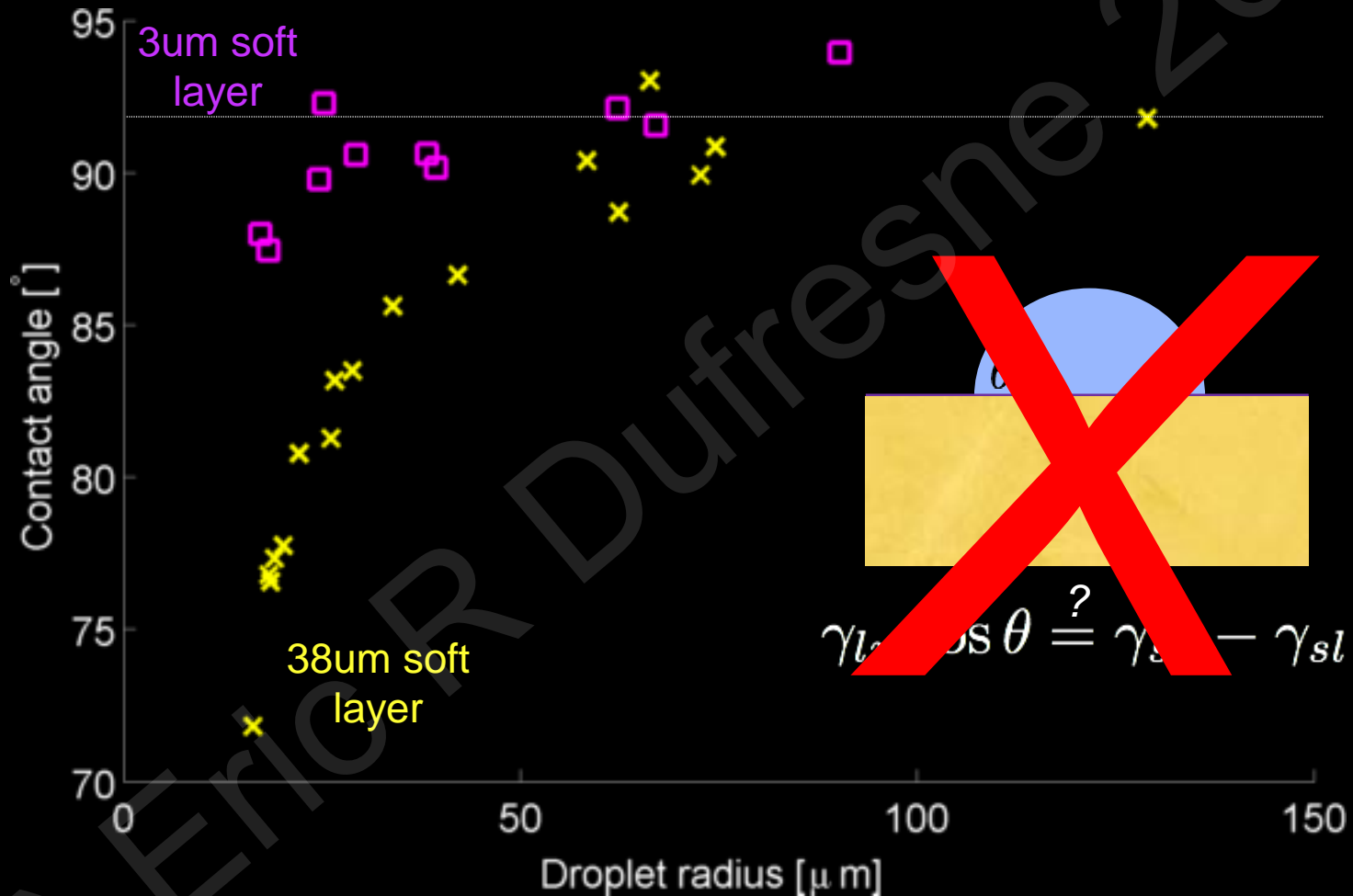
Young-Dupre equation relates contact line geometry and material properties in equilibrium



Thomas Young  
1773-1829

$$\cos \theta = \frac{\gamma_{sv} - \gamma_{sl}}{\gamma_{lv}}$$

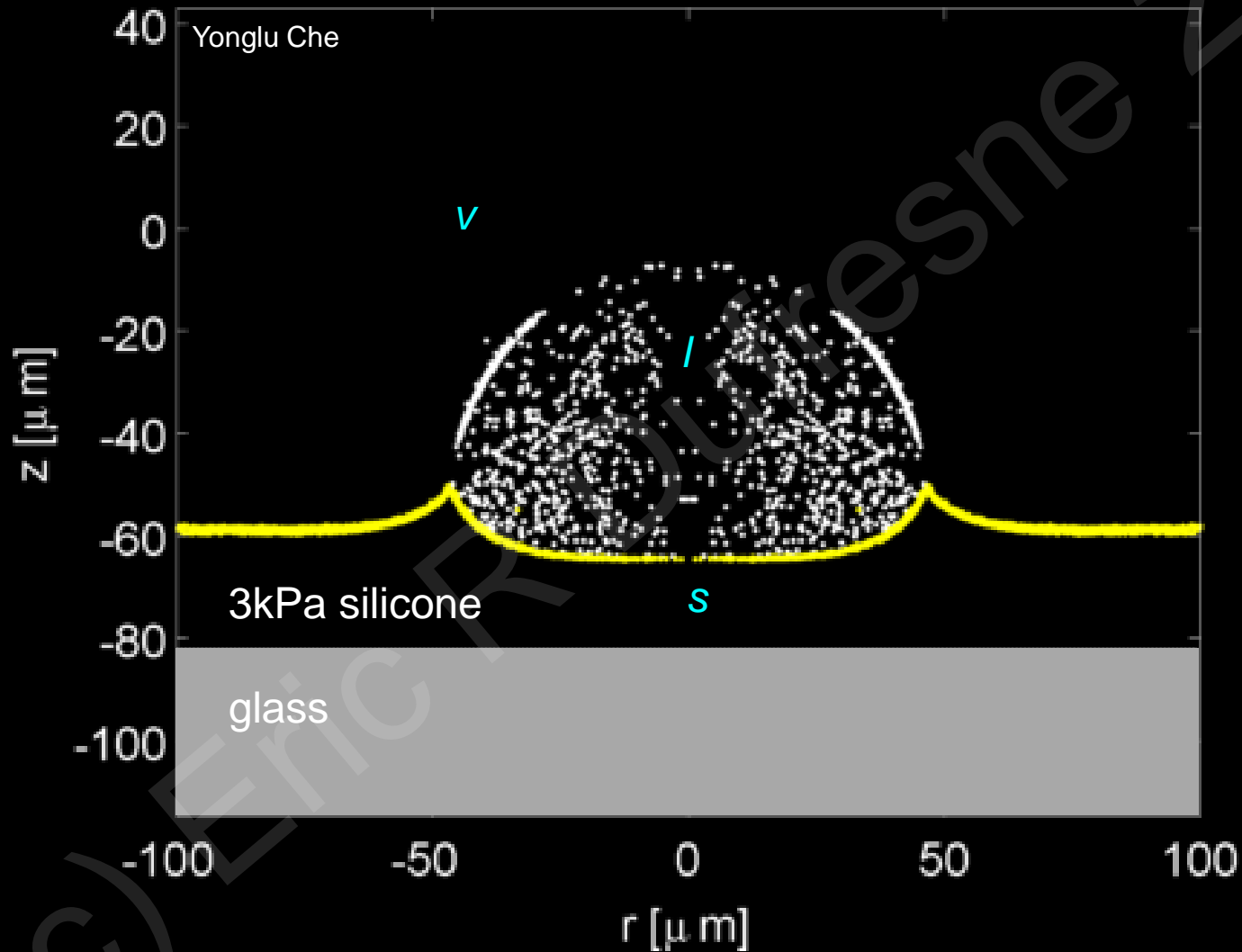
On a soft substrate, apparent contact angle depends on droplet size and thickness of soft layer



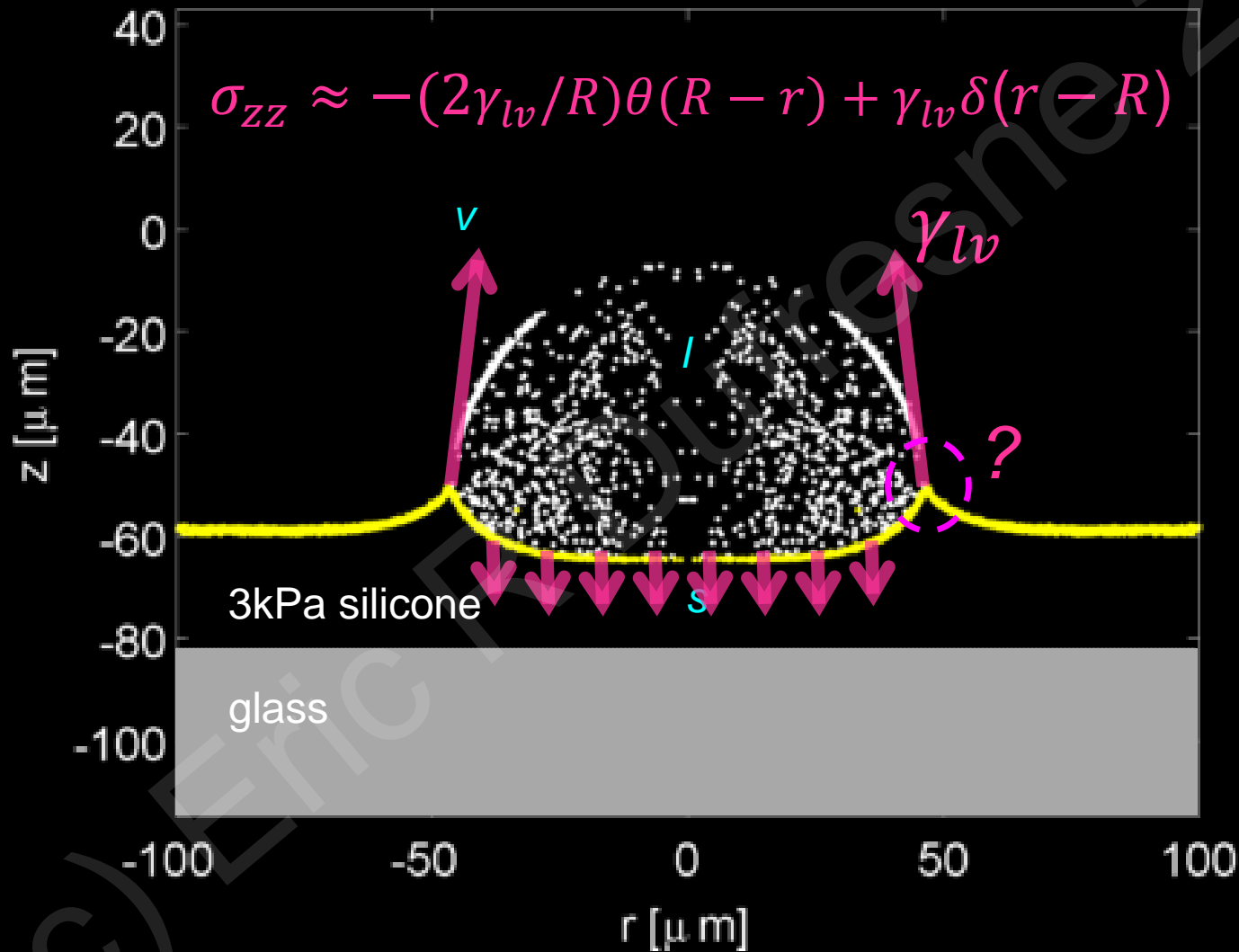
Glycerol drops on silicone (E=3kPa)  
Zygo surface profilometer



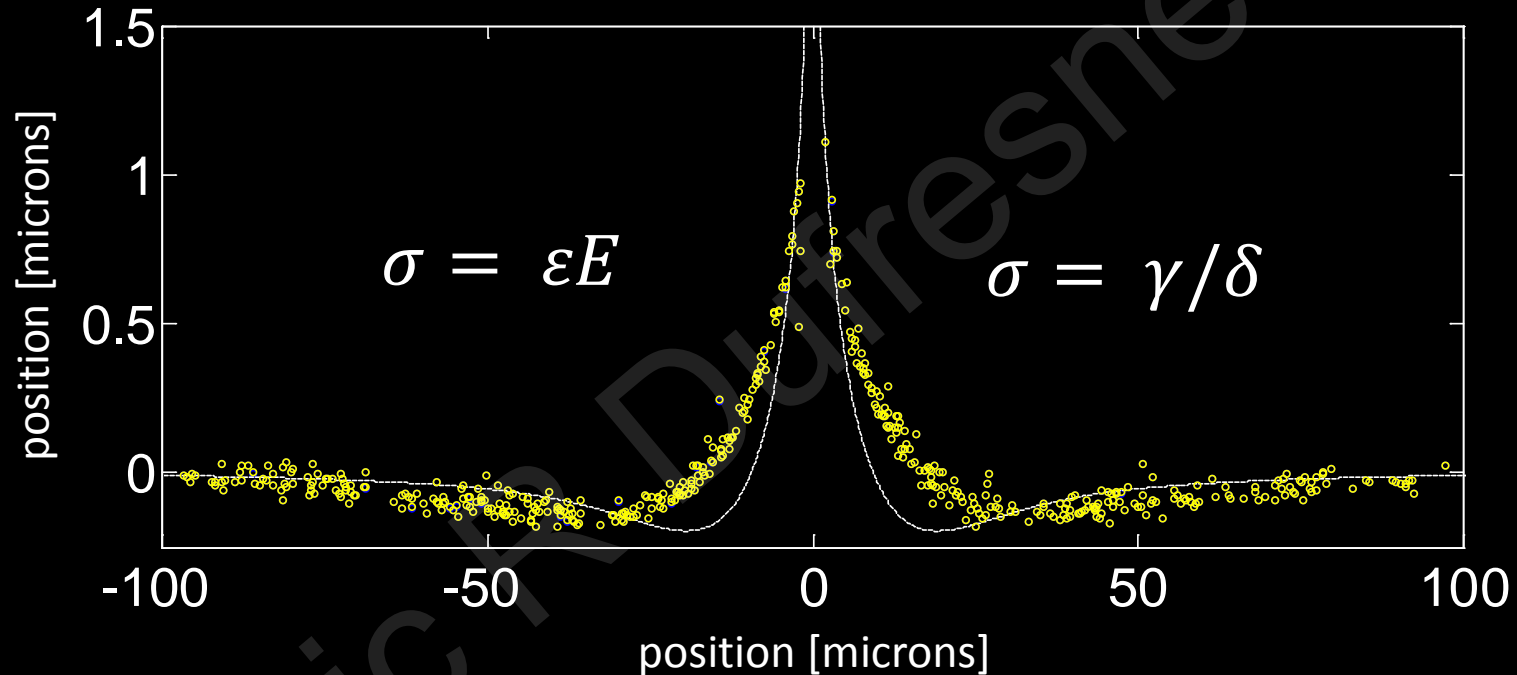
# Droplets Deform Soft Substrates



# Droplets Deform Soft Substrates

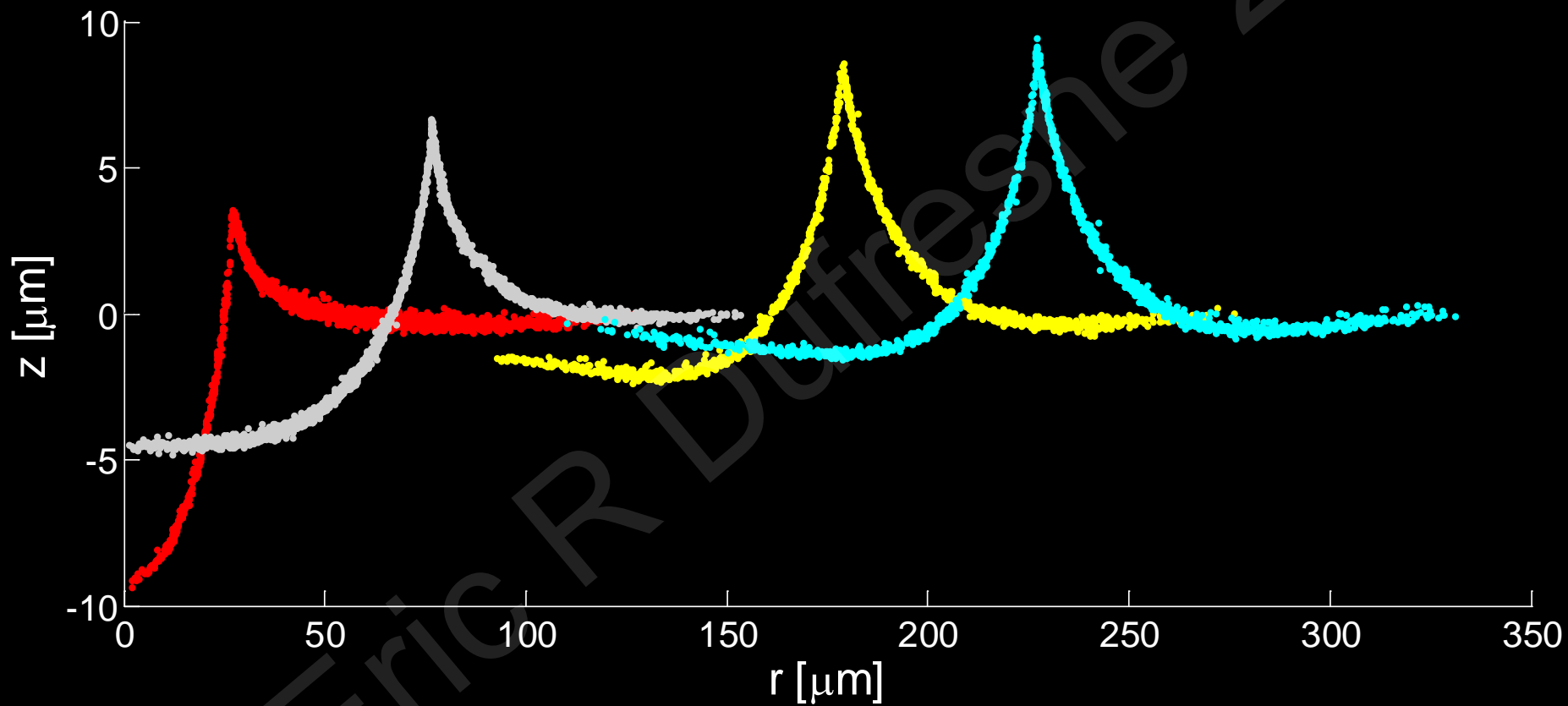


# Elastic Theories Cannot Balance Contact Line Forces

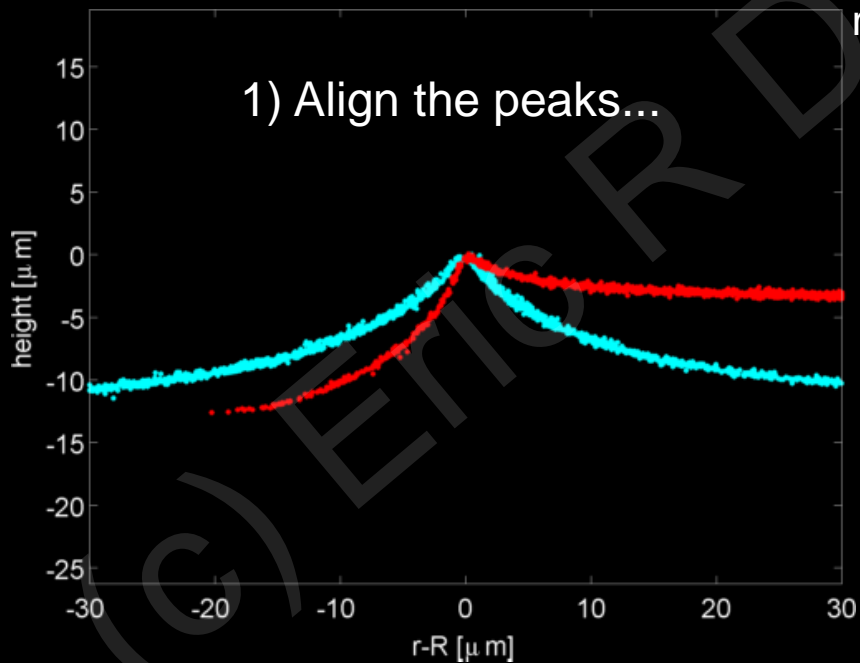
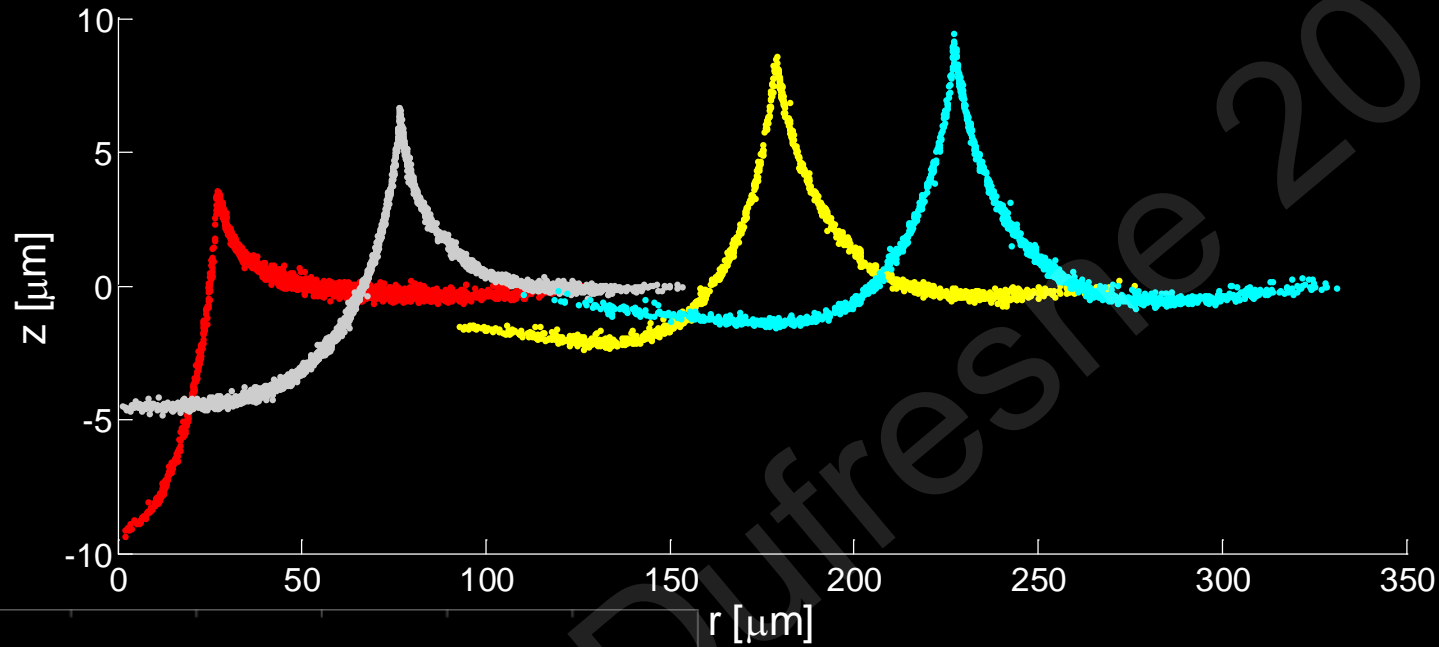


Reasonable estimates for contact line width lead to unreasonable strains and displacements

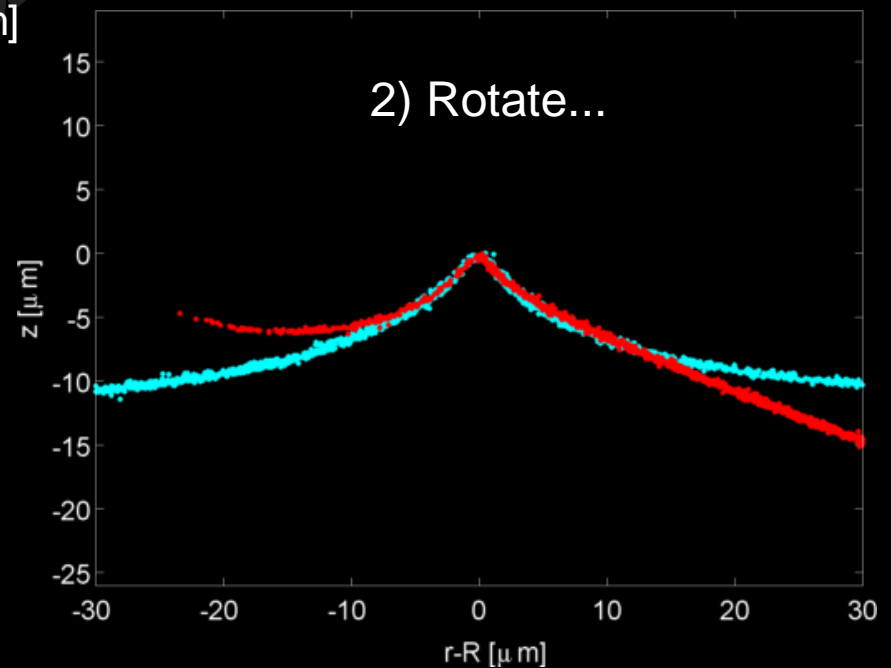
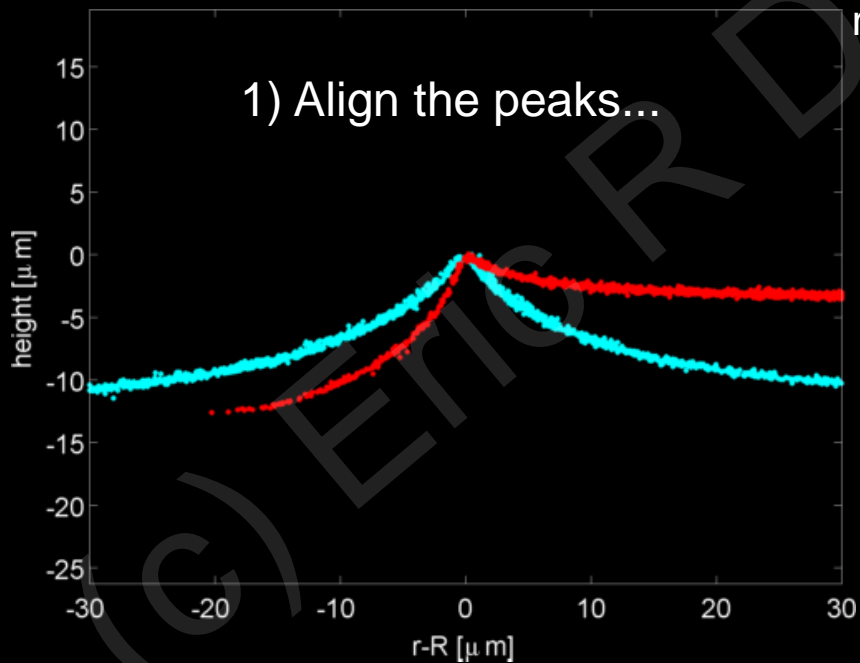
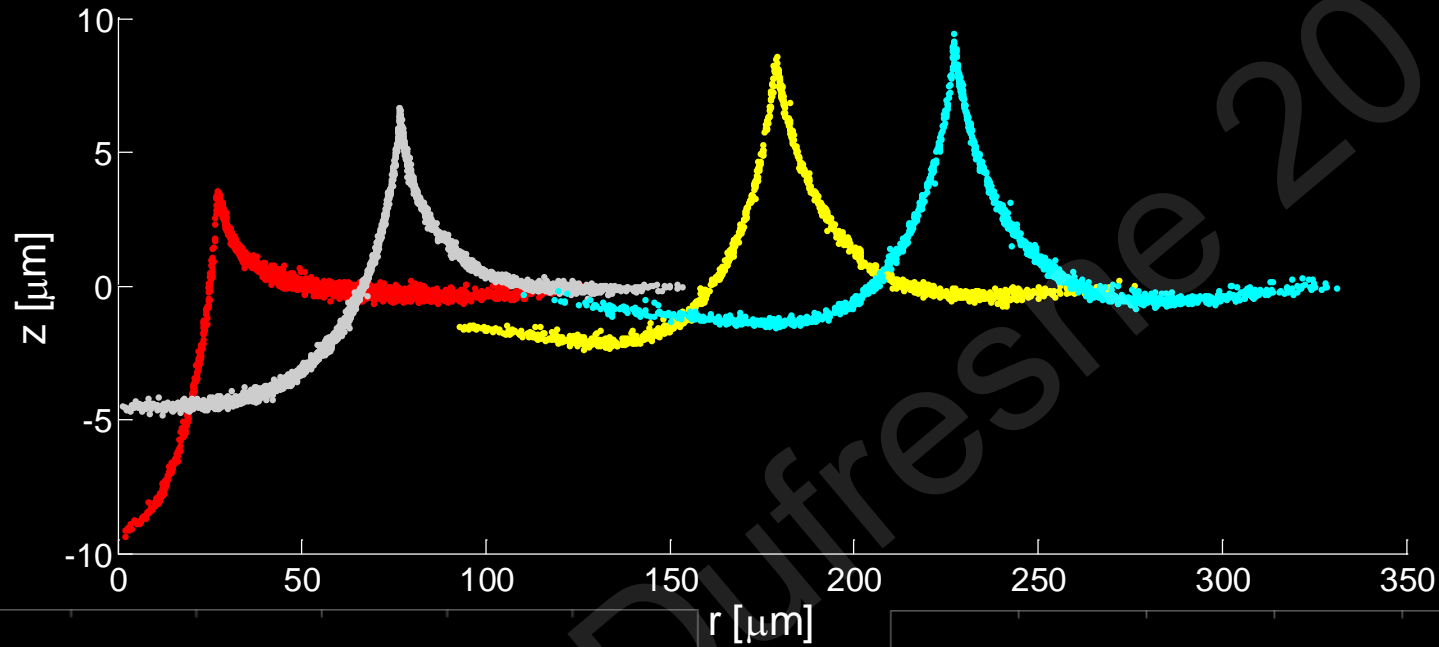
Profiles change dramatically with droplet size



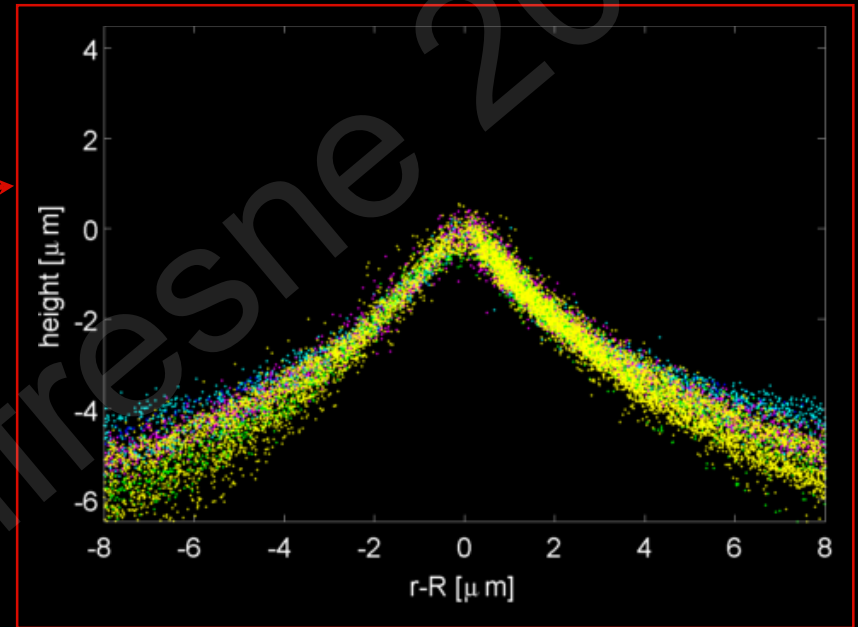
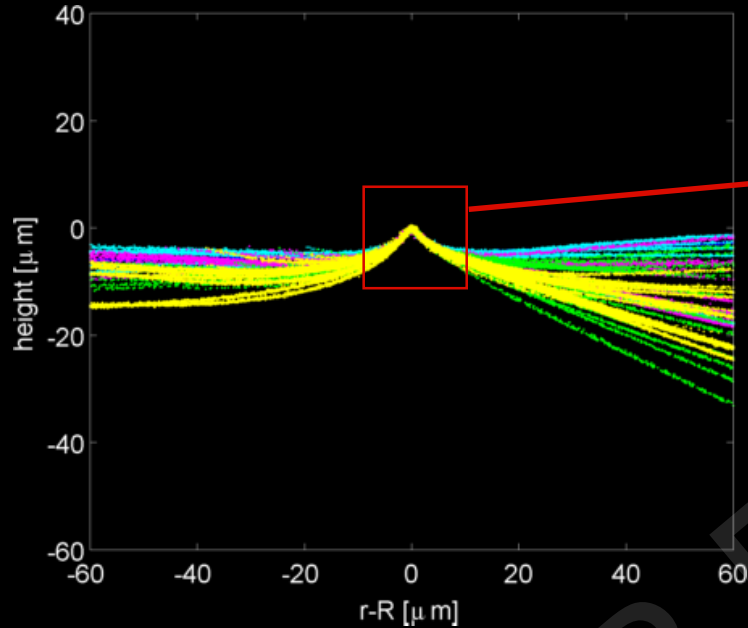
Overall profiles change – but how about the ridge?



Overall profiles change – but how about the ridge?

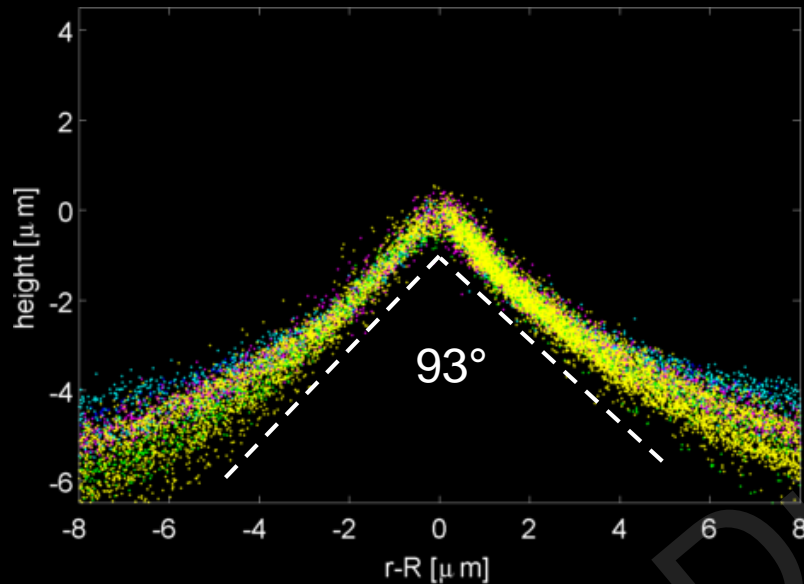


# Ridge shape is universal near contact line

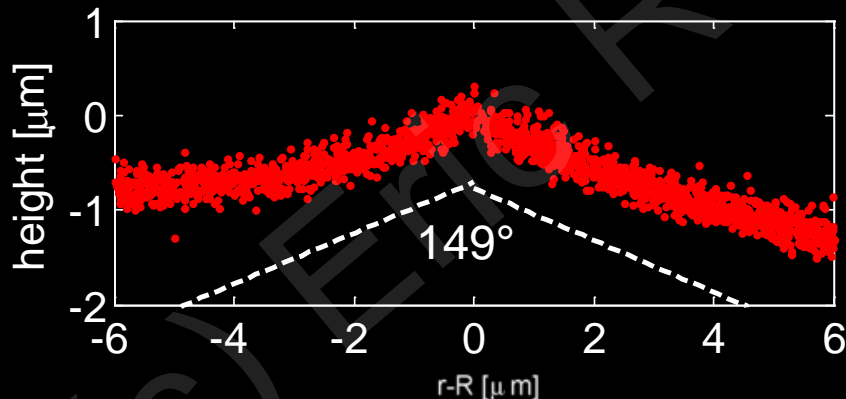


61 glycerol drops  
radii: 18 $\mu\text{m}$  - 1000 $\mu\text{m}$   
Four different substrates: 13.5 - 50 $\mu\text{m}$  thick

# Contact line geometry depends on the wetting fluid



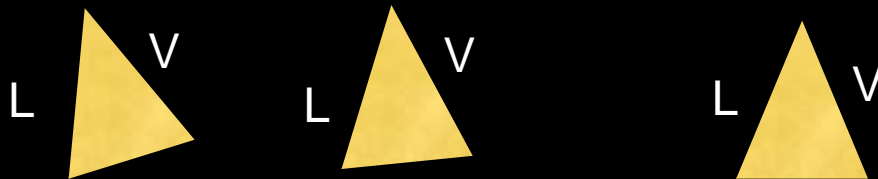
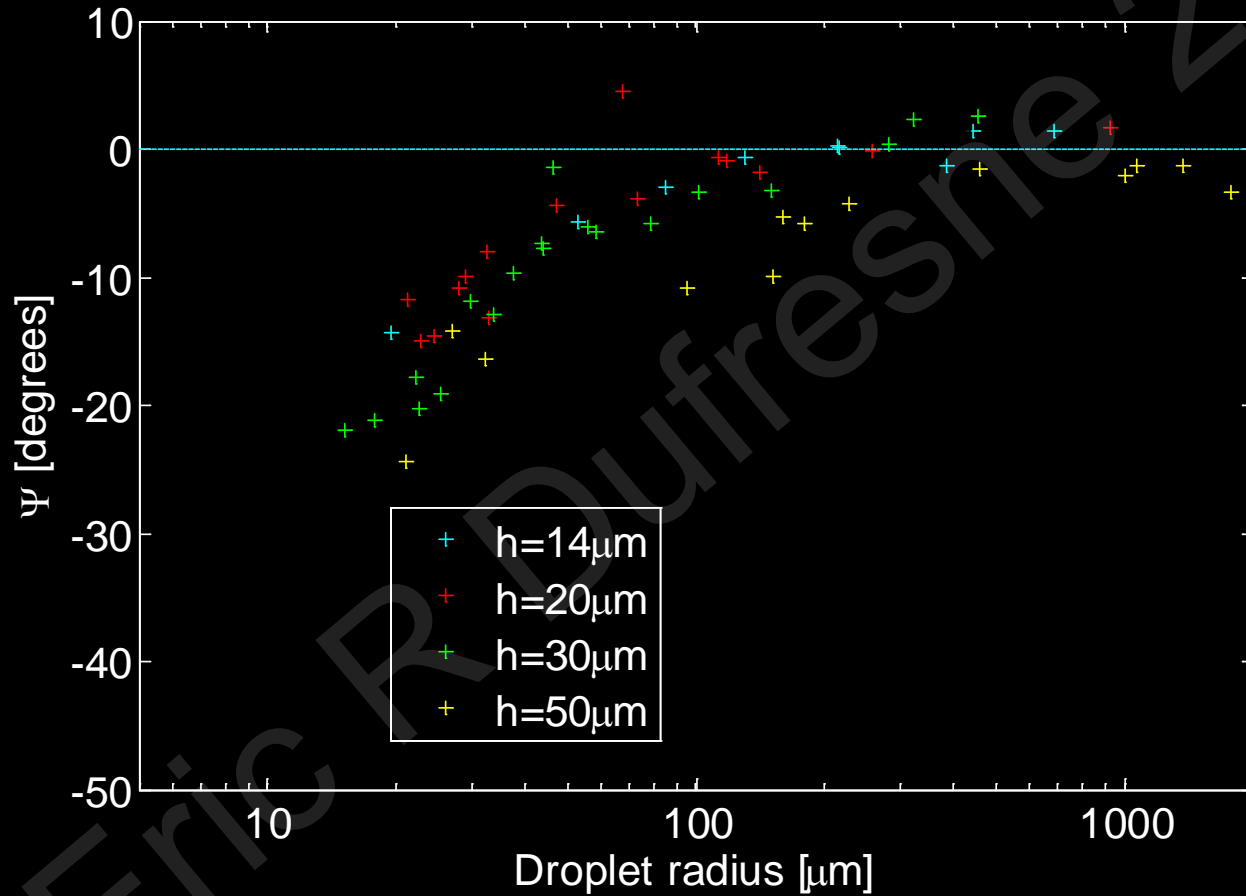
glycerol  
61 drops  
radii: 18 $\mu\text{m}$  - 1000 $\mu\text{m}$   
substrates: 13.5 - 50 $\mu\text{m}$  thick



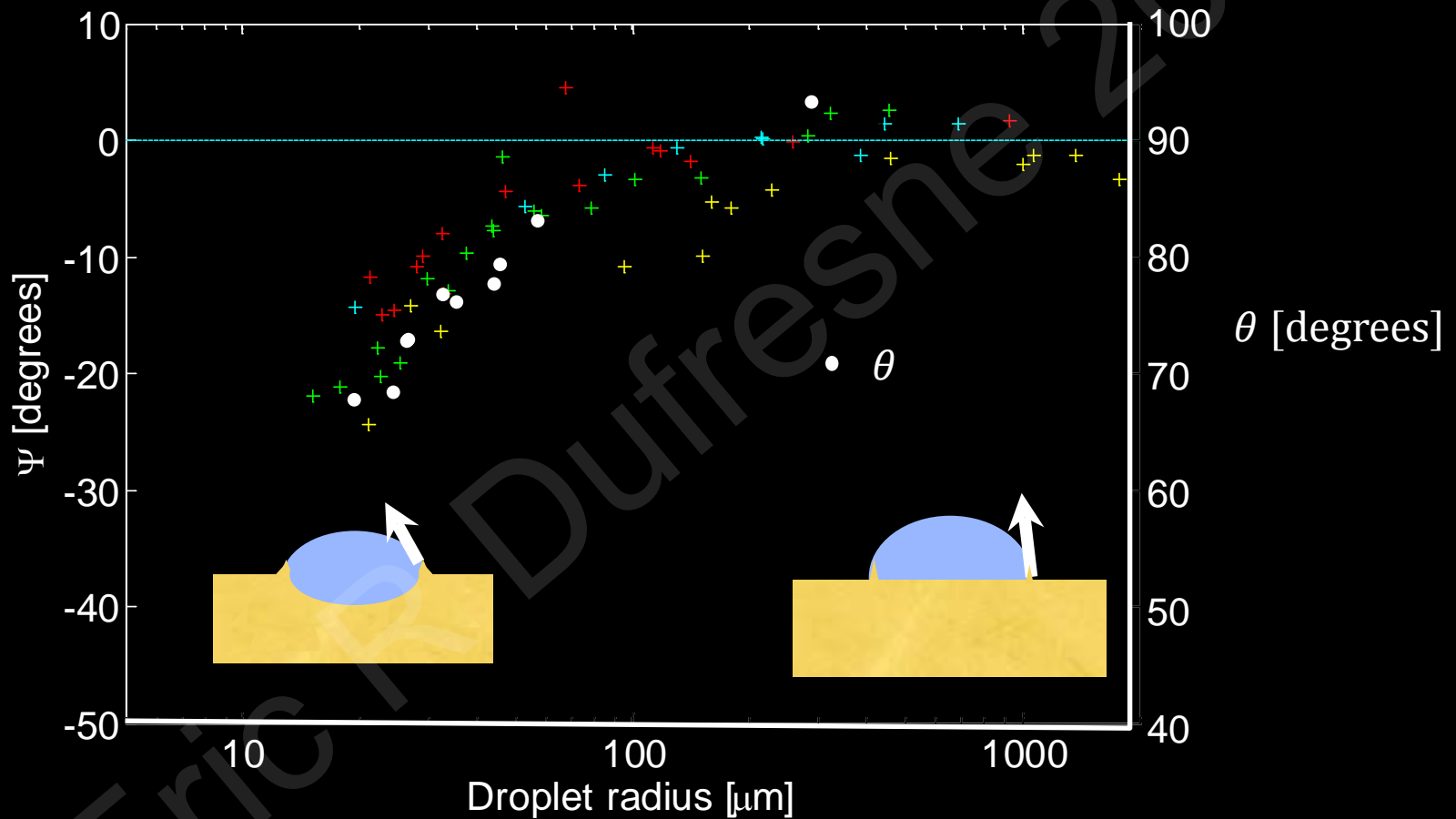
fluorinert fc-70  
14 drops  
radii: 140 $\mu\text{m}$  - 270 $\mu\text{m}$   
substrate: 23  $\mu\text{m}$  thick



# Cusp rotates as droplets get smaller



# Macroscopic contact angle follows rotation of cusp



Angles between all three interfaces are fixed!

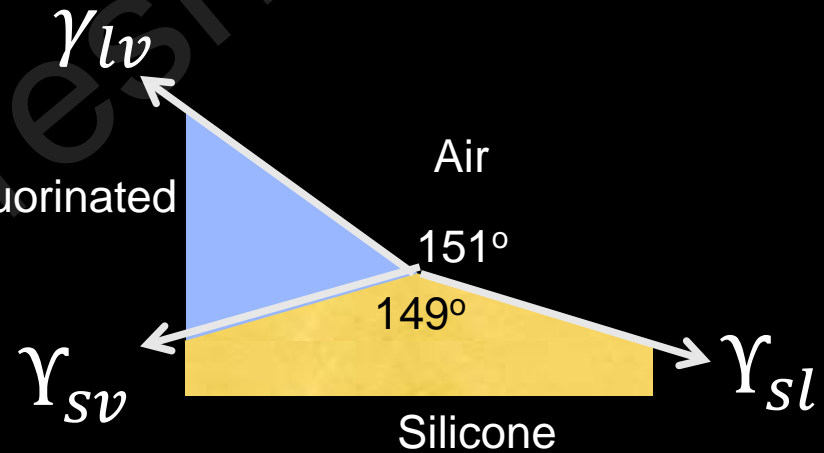
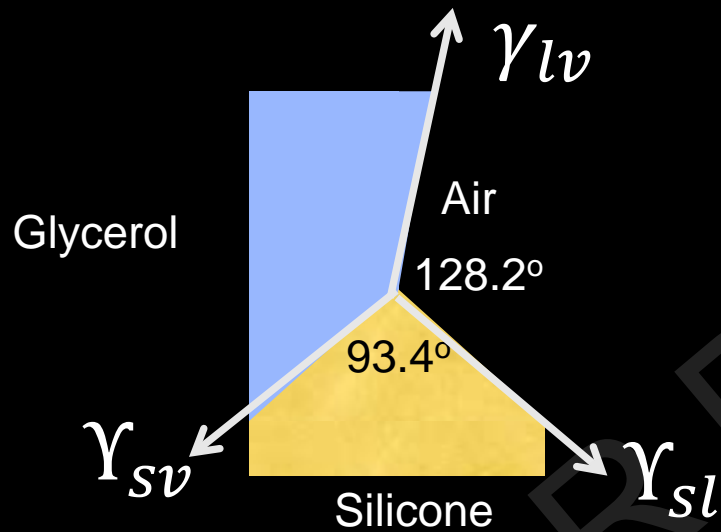
While apparent contact angle depends on boundary conditions...  
microscopic configuration of interfaces is universal



## Key Experimental Observations

- Young's law doesn't work on a 3KPa silicone substrate when glycerol droplets are smaller than about 100 microns. The apparent contact angle drops as the droplet gets smaller.
- For droplets much bigger than 100 microns, you get a size independent contact angle. This contact angle matches that of much stiffer silicone, of order 1MPa, about 90 degrees.
- Within two microns of the contact line, all the interfaces are straight and meet each other at fixed orientations. These orientations depend on the liquid.

Hypothesis: geometry at contact line is determined by a vector balance of interfacial stresses

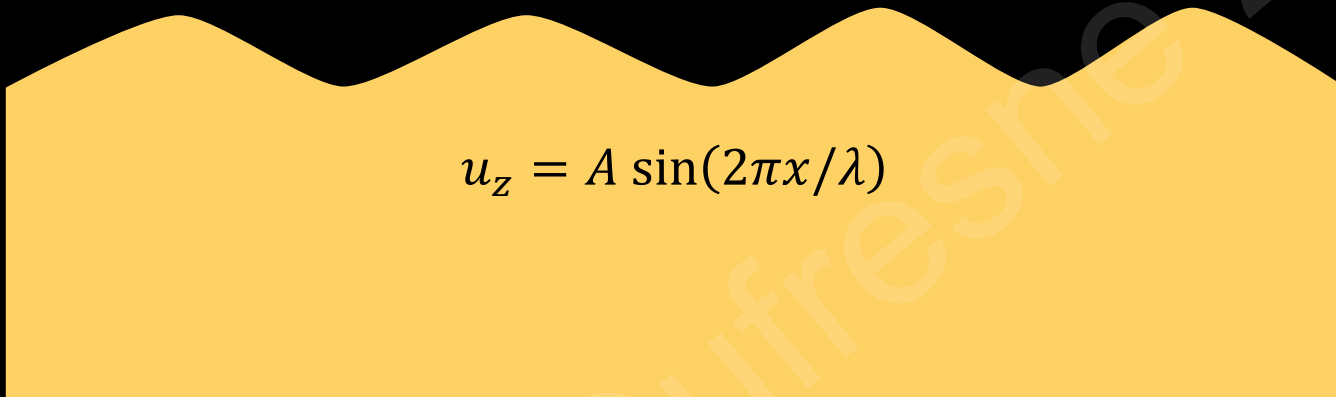


$\gamma_{lv}$ : l-v surface tension

$\gamma_{sv}$ : s-v surface tension

$\gamma_{sl}$ : s-l surface tension

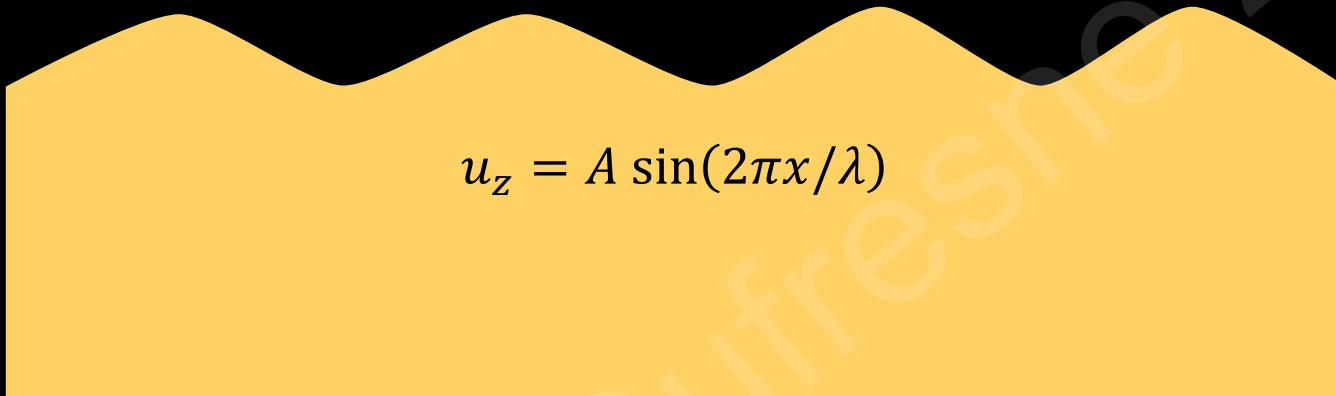
# Deformation of a linear elastic solid surface



Elastic restoring force:  $\sigma_E = \varepsilon E \sim AE/\lambda$

# Flattening of a linear elastic solid by surface tension

Long Ajdari 1996, Jerison Dufresne 2011, Jagota 2012

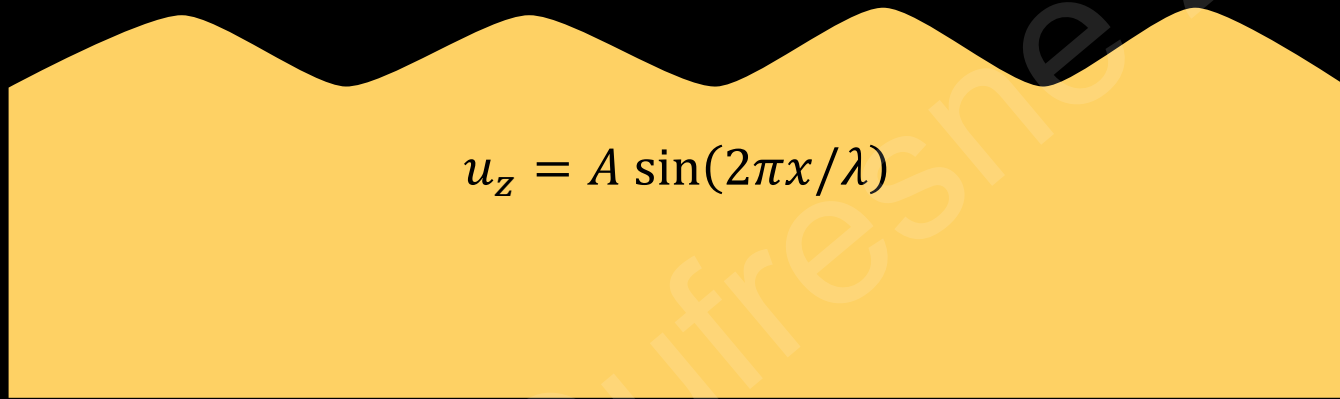


Elastic restoring force:  $\sigma_E = \varepsilon E \sim AE / \lambda$

Capillary force (LaPlace):  $\sigma_\gamma \sim \Upsilon A / \lambda^2$

$\Upsilon$ : solid surface tension

# Balance of Elasticity and Capillarity Defines a Length scale



$$\frac{\sigma_E}{\sigma_\gamma} \sim \frac{\lambda}{\gamma/E}$$

$$l = \gamma/E$$

Elastocapillary Length

$$\lambda \gg \gamma/E$$

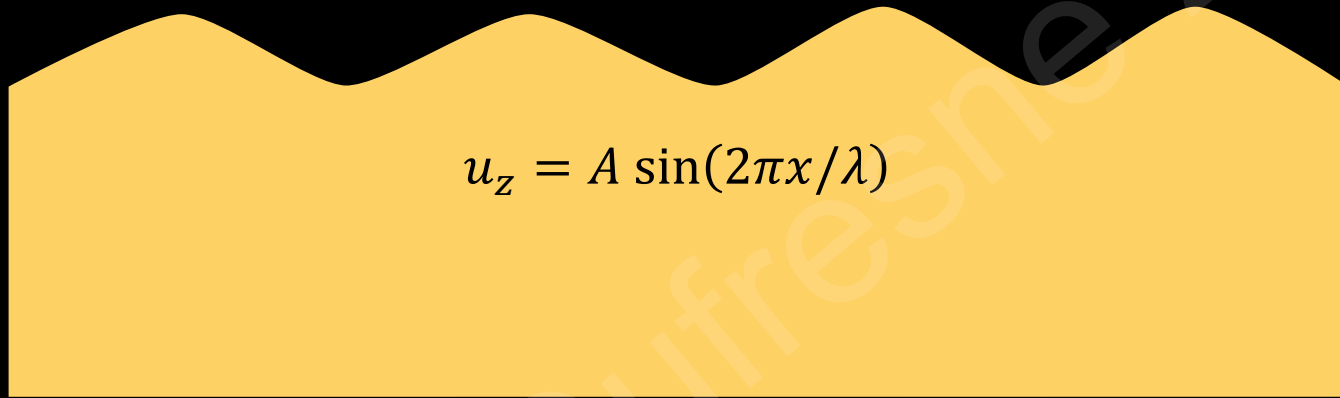
$$\lambda \ll \gamma/E$$

Elasticity Dominates

Surface Tension Dominates



# Capillarity Dominates at Short Length Scales on Soft Materials



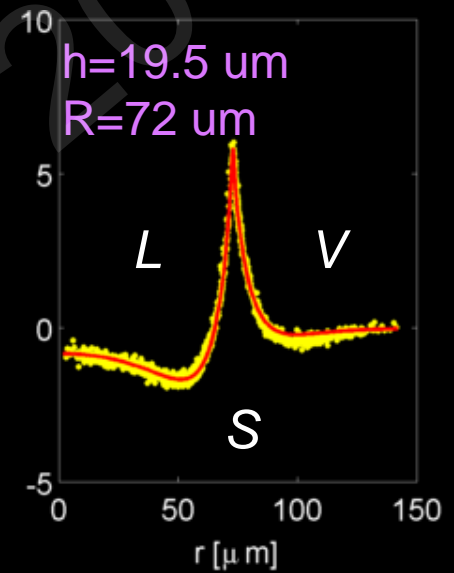
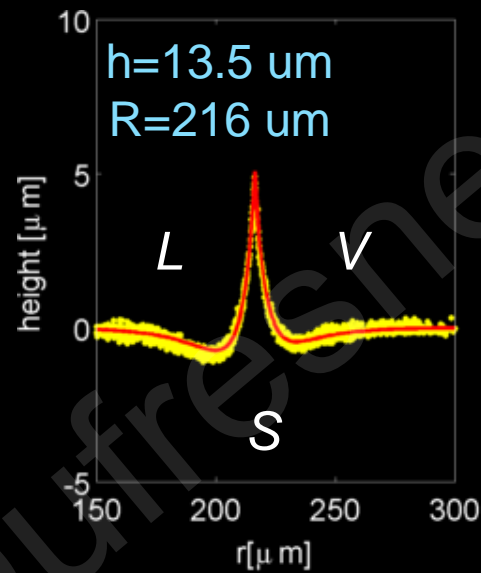
$$\gamma = 0.03 \text{ N/m}$$

$$\gamma/E = 0.1 \text{ \AA} \text{ for } E = 3 \text{ GPa}$$

$$\gamma/E = 10 \text{ nm for } E = 3 \text{ MPa}$$

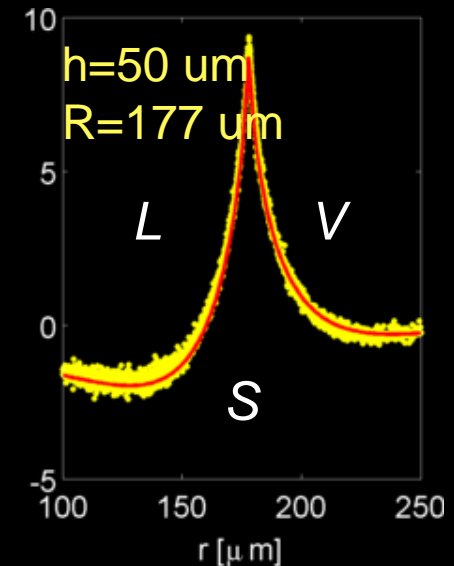
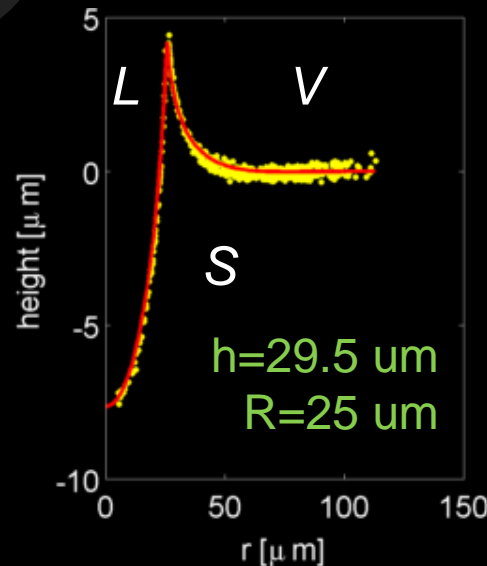
$$\gamma/E = 10 \text{ }\mu\text{m for } E = 3 \text{ kPa}$$

# Linear Elasticity Plus Solid Surface Tension Captures Profiles

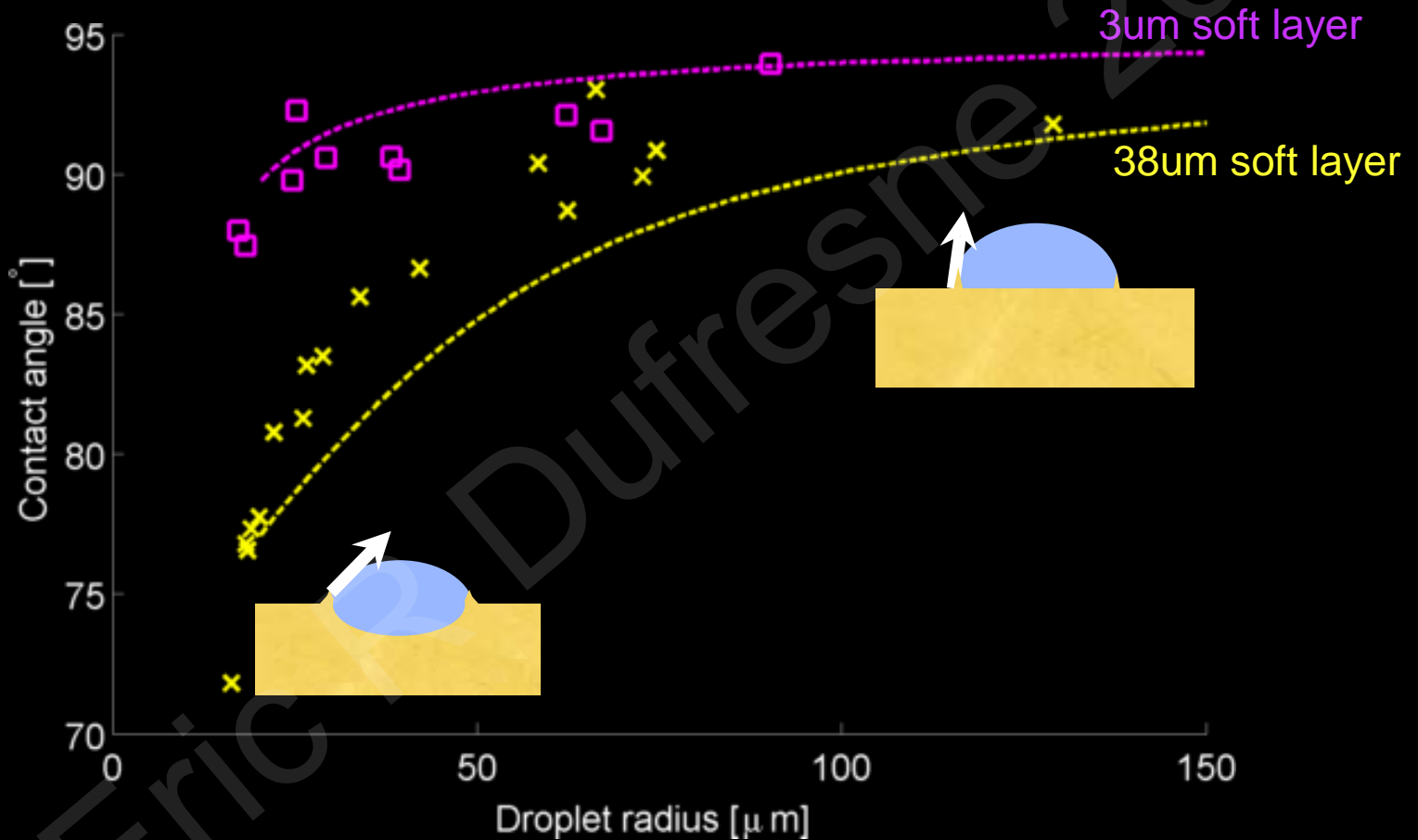


*Sharp features near contact line are controlled by surface tension.*

*Far-field determined by elasticity*



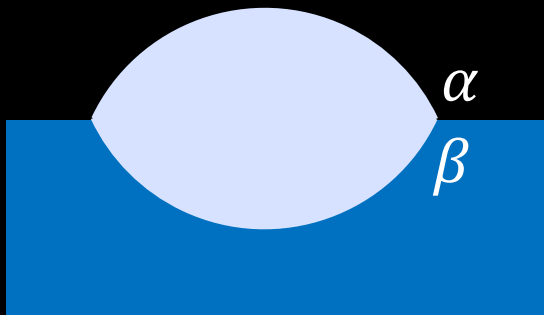
# Linear Elasticity Plus Solid Surface Tension Predicts Change in Apparent Contact Angle



Glycerol drops on silicone ( $E=3\text{kPa}$ )

# Wetting on Deformable Solids

Neumann  
(liquid on liquid)

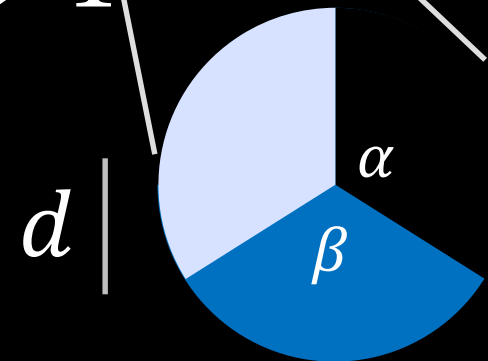


$$\gamma/ER \ll 1$$

Young-Dupre  
(liquid on rigid solid)



$$\gamma/ER \gg 1$$



$$\gamma/Ed \gg 1$$

Theory and preliminary expts:  
Jerison *et al* *Physical Review Letters* 2011  
Style *et al* *Soft Matter* 2012

Breakdown of Young-Dupre  
Style *et al* *Physical Review Letters* 2013

Drop movement  
Style *et al* *PNAS* 2013

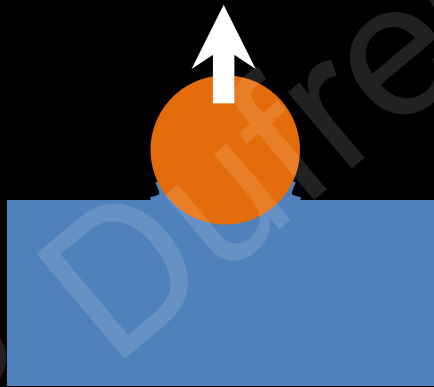
# Three Foundational Theories of Interfacial Mechanics

*Young-Dupre (18XX)*



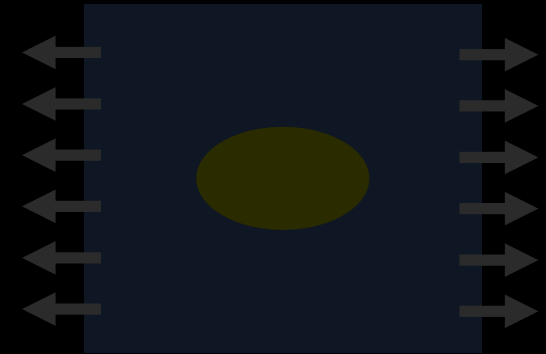
wetting

*JKR (1971)*



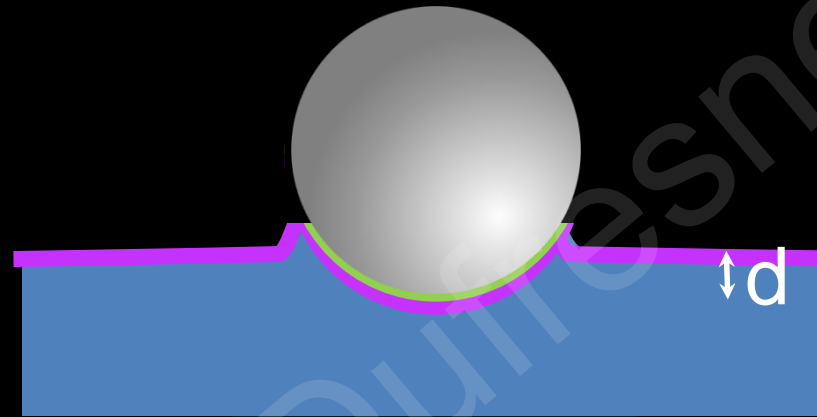
adhesion

*Eshelby (1957)*



composites,  
fracture,  
dislocations

Johnson, Kendall & Roberts (1971) – ‘JKR’

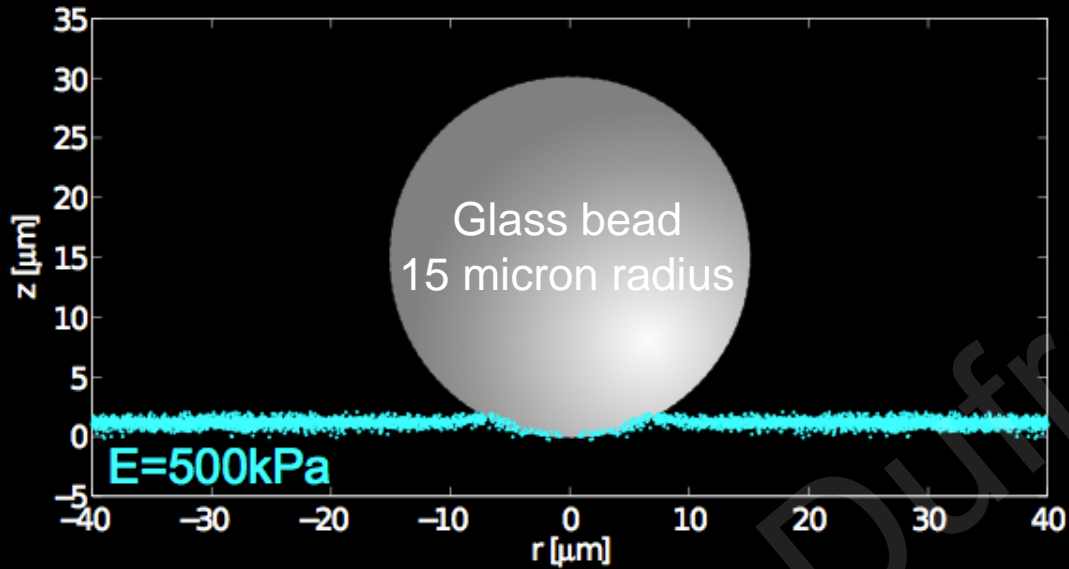


Adhesion Energy,  $W = \gamma_{sp} - \gamma_{sv} - \gamma_{pv}$

Substrate Elasticity,  $E$

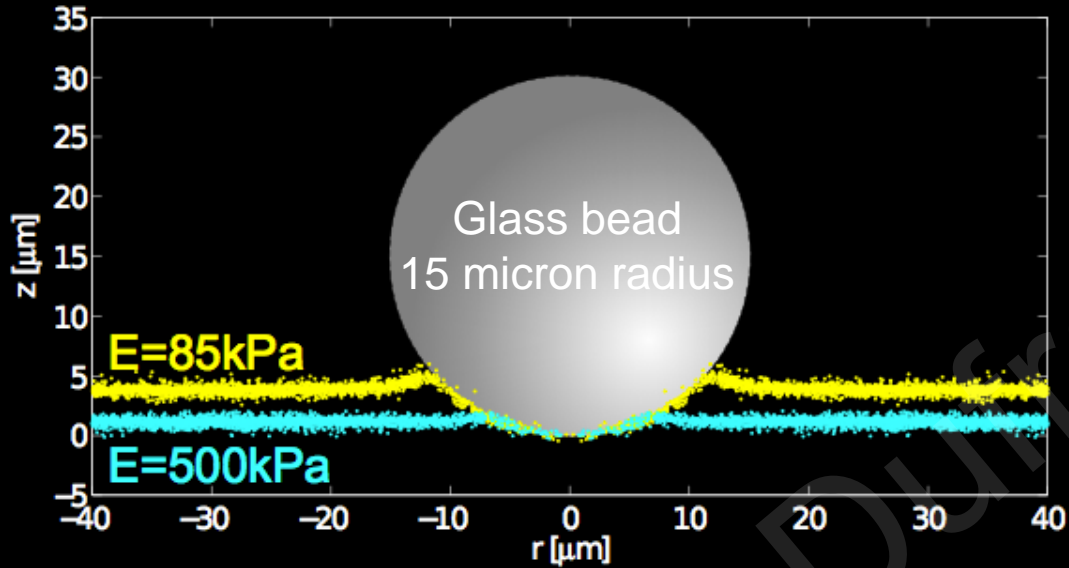
Substrate surface tension,  $\gamma_{sv}, \gamma_{sp}$ ?

# Zero-force indentation for different stiffness substrates



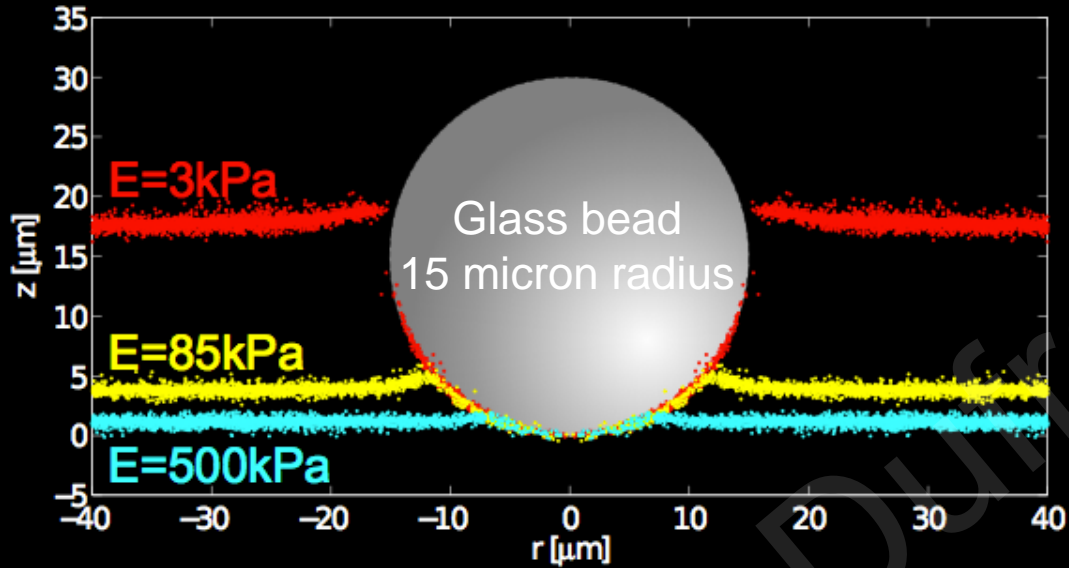
© Eric R Dufresne 2015

# Zero-force indentation for different stiffness substrates

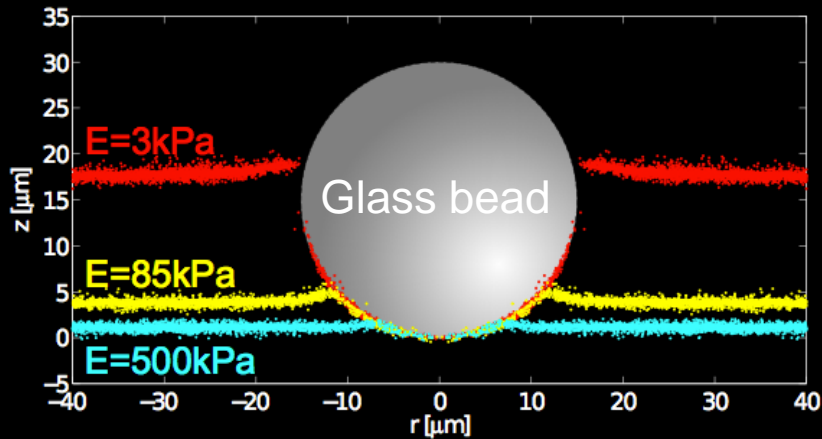




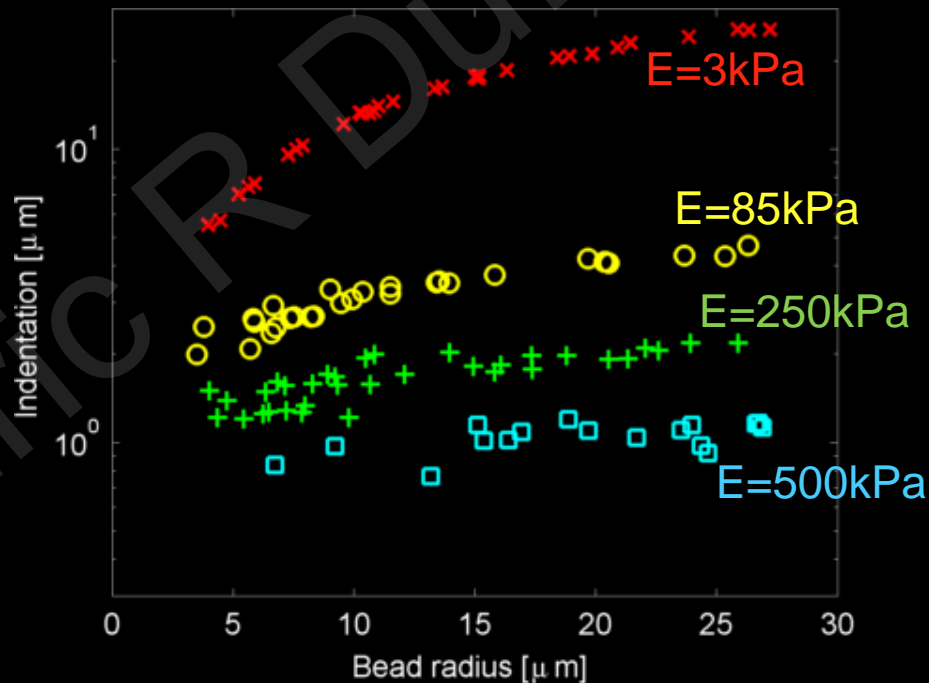
# Zero-force indentation for different stiffness substrates



# Zero-force indentation for different stiffness substrates

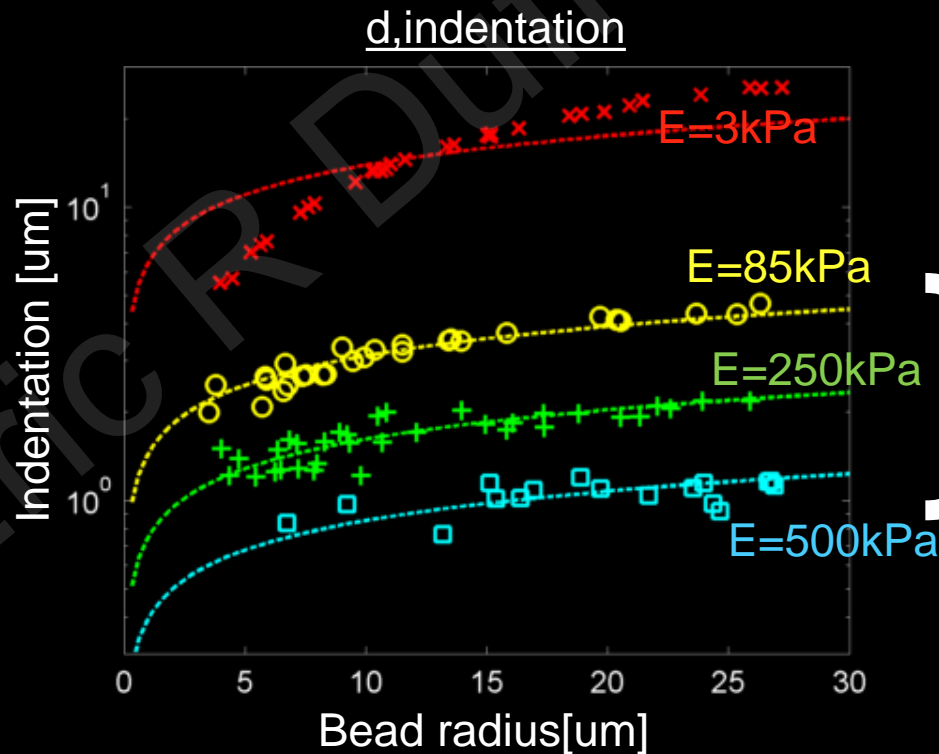


$d$ , indentation



# Comparing results with JKR

$$d = \left( \frac{\sqrt{3}W(1 - \nu^2)}{2E} \right)^{2/3} R^{1/3}$$

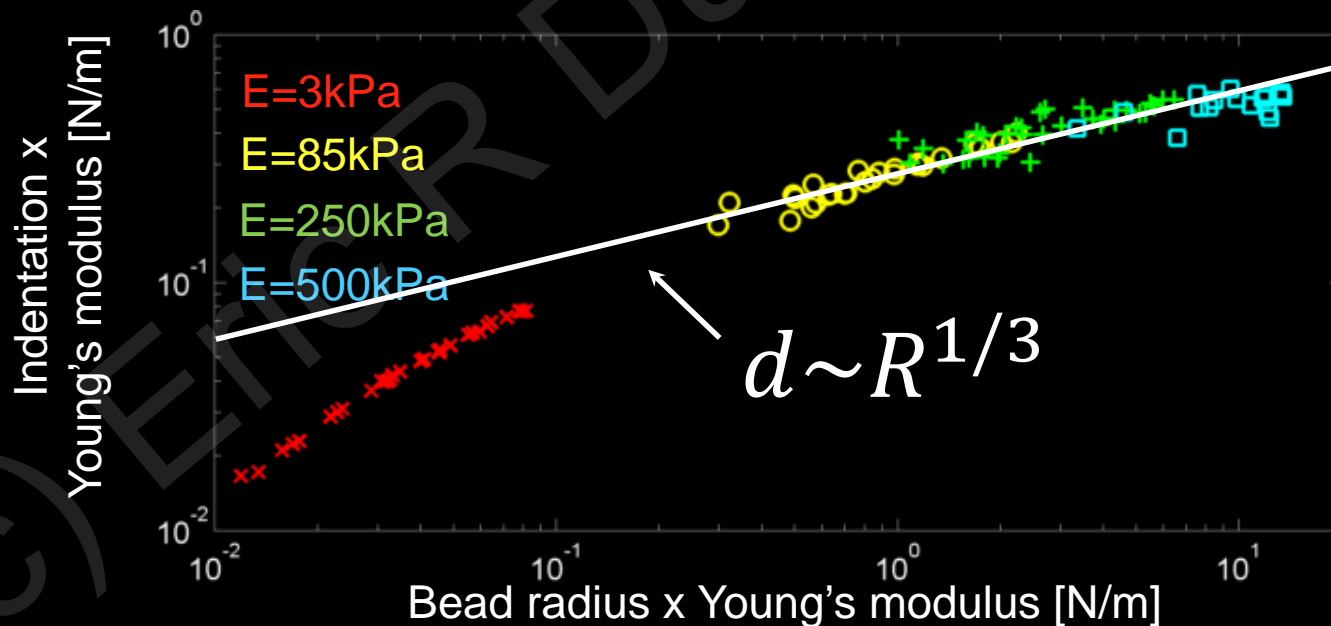


$W \sim 25\text{mN/m}$

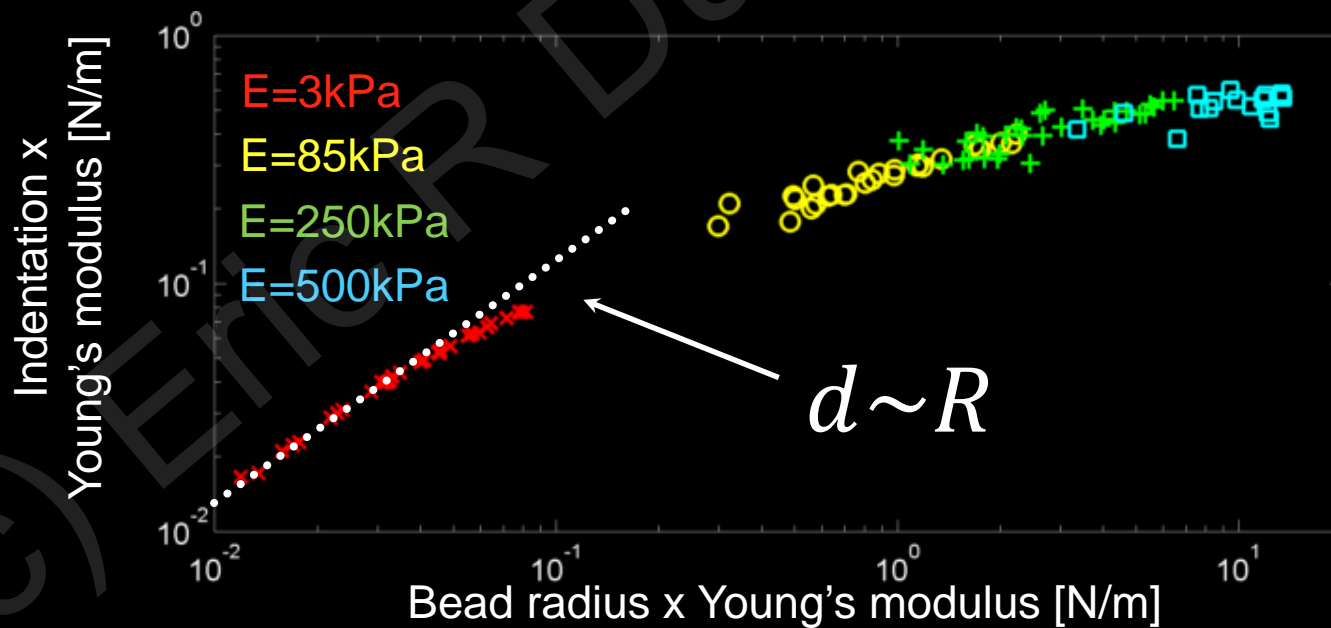
$W \sim 70\text{mN/m}$

JKR collapses the data, but scaling changes for small particles and soft surfaces

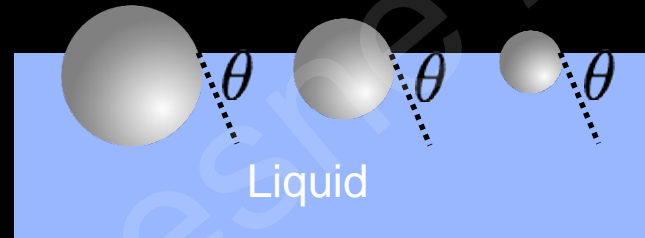
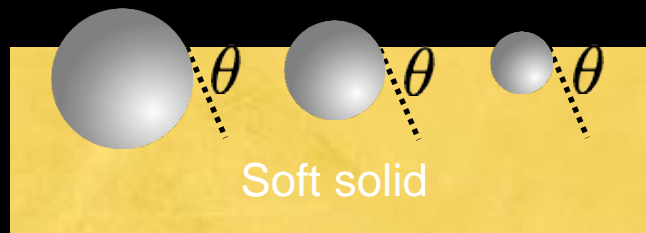
$$\text{JKR: } dE = \left( \frac{\sqrt{3}W(1-\nu^2)}{2} \right)^{2/3} (RE)^{1/3}$$



Indentation proportional to bead radius for small beads



Indentation,  $d \sim R$  implies constant contact angle



$$\gamma_{lv} \cos \theta = \gamma_{sv} - \gamma_{sl}$$

For small particles at zero force, the indentation depth is given by Young-Dupre, just like a colloidal particle on a fluid interface

Style *et al* *Nature Communications* (2013)

Jensen *et al* ...preprint to appear soon on arXiv

# JKR plus surface tension fits data

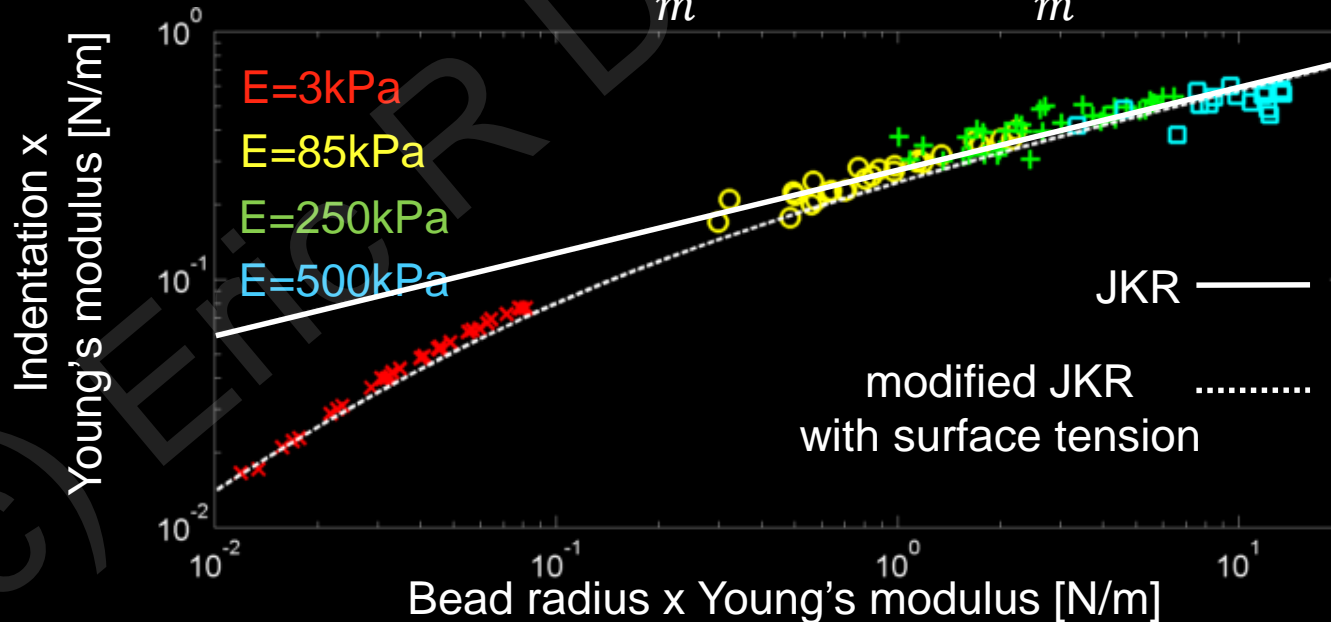
Minimize total energy (a la Carillo/Raphael/Dobrynin 2010):

Elastic energy + Adhesion Energy + Surface Tension

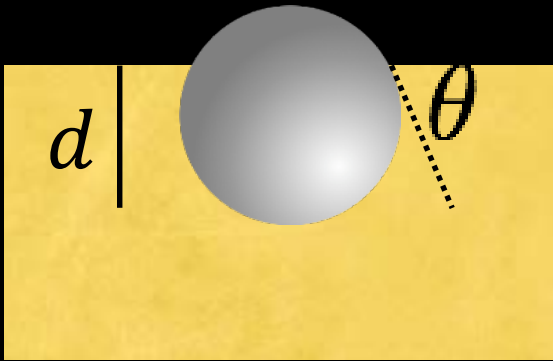
(from JKR)

$$\gamma_{sv} \Delta A$$

$$W = 71 \frac{mN}{m}, \quad \gamma_{sv} = 45 \frac{mN}{m}$$



In the limit of small beads, our scaling predicts...



$$d = WR/\gamma_{sv}$$

equivalently...

$$\gamma_{sv} \cos \theta = W - \gamma_{sv}$$

'Smells' like Young-Dupre

for  $\gamma_{sv} = \gamma_{sv}$ ,

$$\gamma_{sv} \cos \theta = \gamma_{sp} - \gamma_{pv}$$

Young-Dupre with soft substrate in the place of the liquid



# Adhesion Summary

- For large particles,  $\gamma/ER \ll 1$ , the classic balance of surface energy and elasticity by JKR accurately describes contact mechanics of soft substrate
- For small particles,  $\gamma/ER \gg 1$ , the indentation depth is given by Young-Dupre, just like a colloidal particle on a fluid interface.
- Again, surface tension swamps elasticity for  $\gamma/ER \gg 1$

Style *et al* *Nature Communications* (2013)

Latest coming to the *arXiv* next week!

# Three Foundational Theories of Interfacial Mechanics

*Young-Dupre (18XX)*



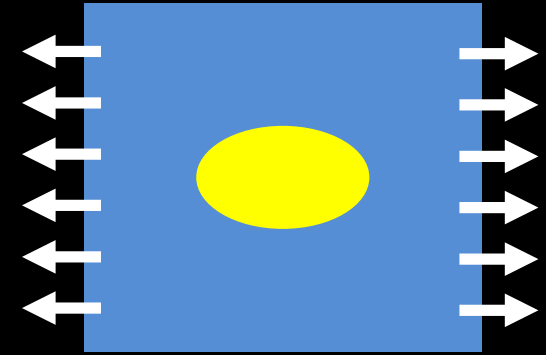
wetting

*JKR (1971)*



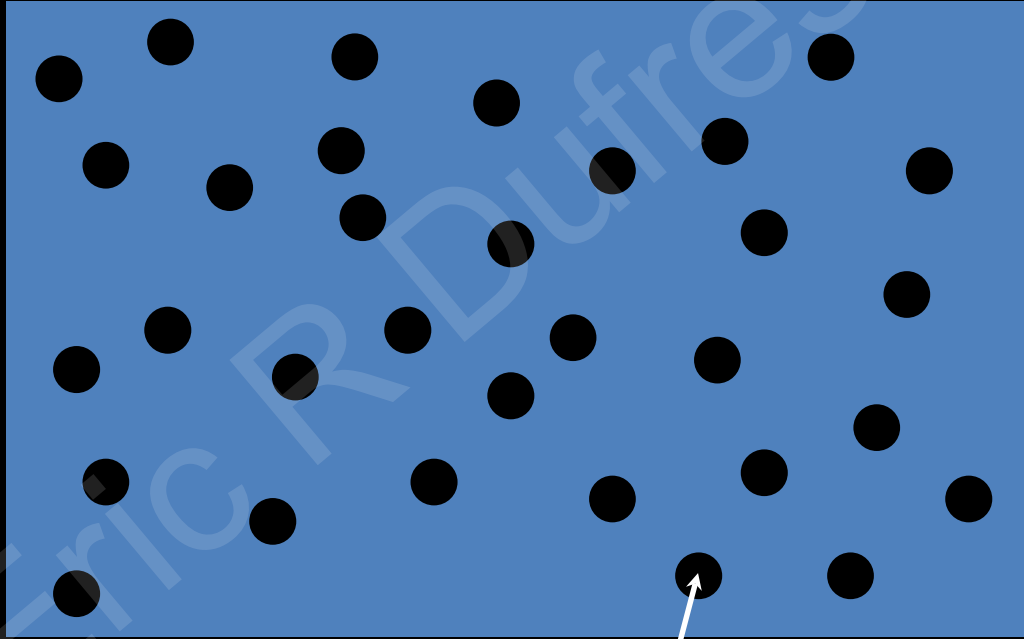
adhesion

*Eshelby (1957)*



composites,  
fracture,  
dislocations





fluid

(C) Eric R. Dufresne 2015

0%

5%

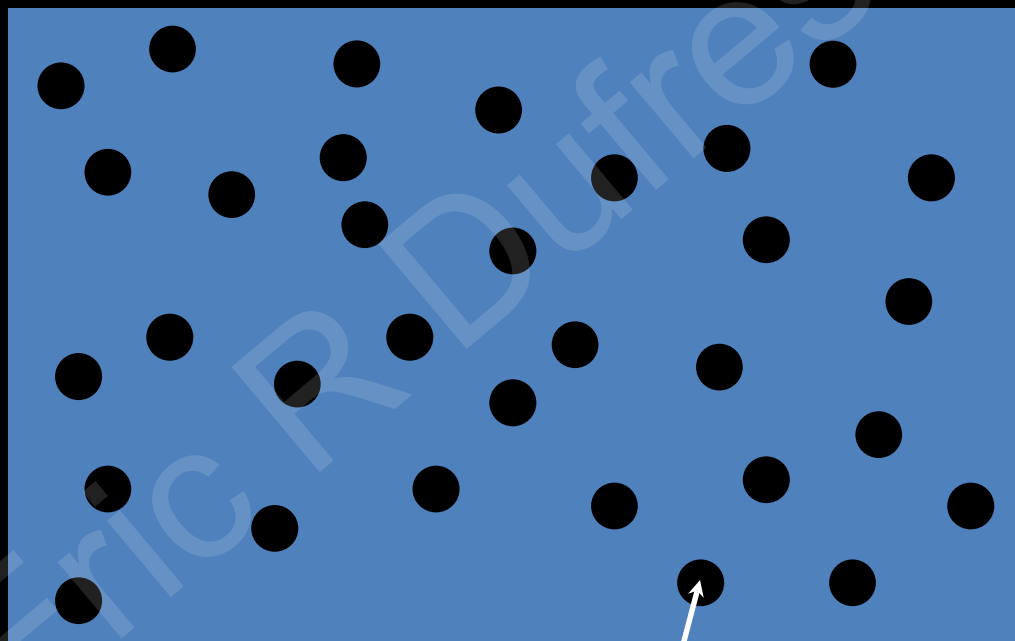
10%

15%

20% v/v

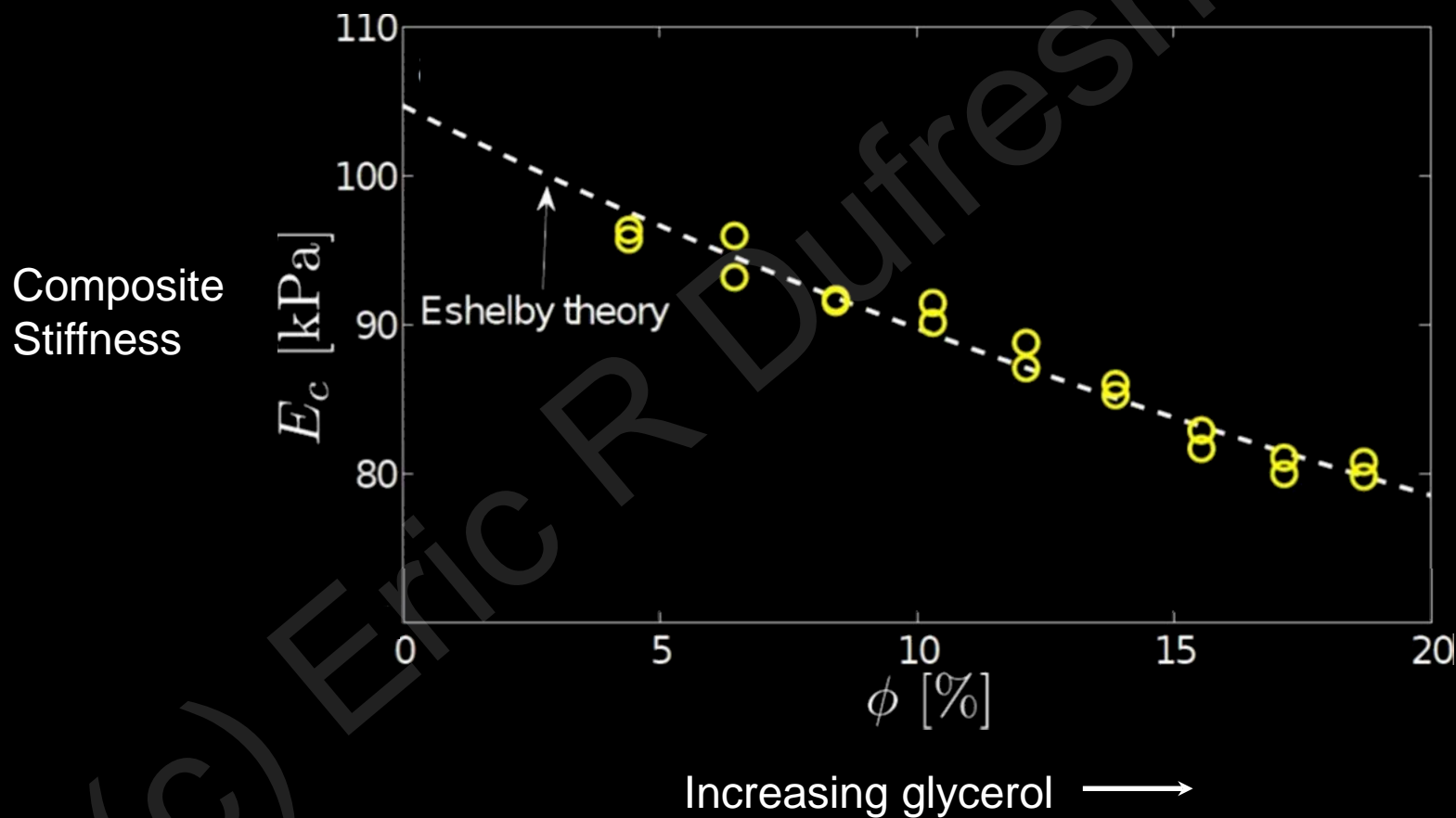


micron scale  
glycerol  
droplets in  
PDMS



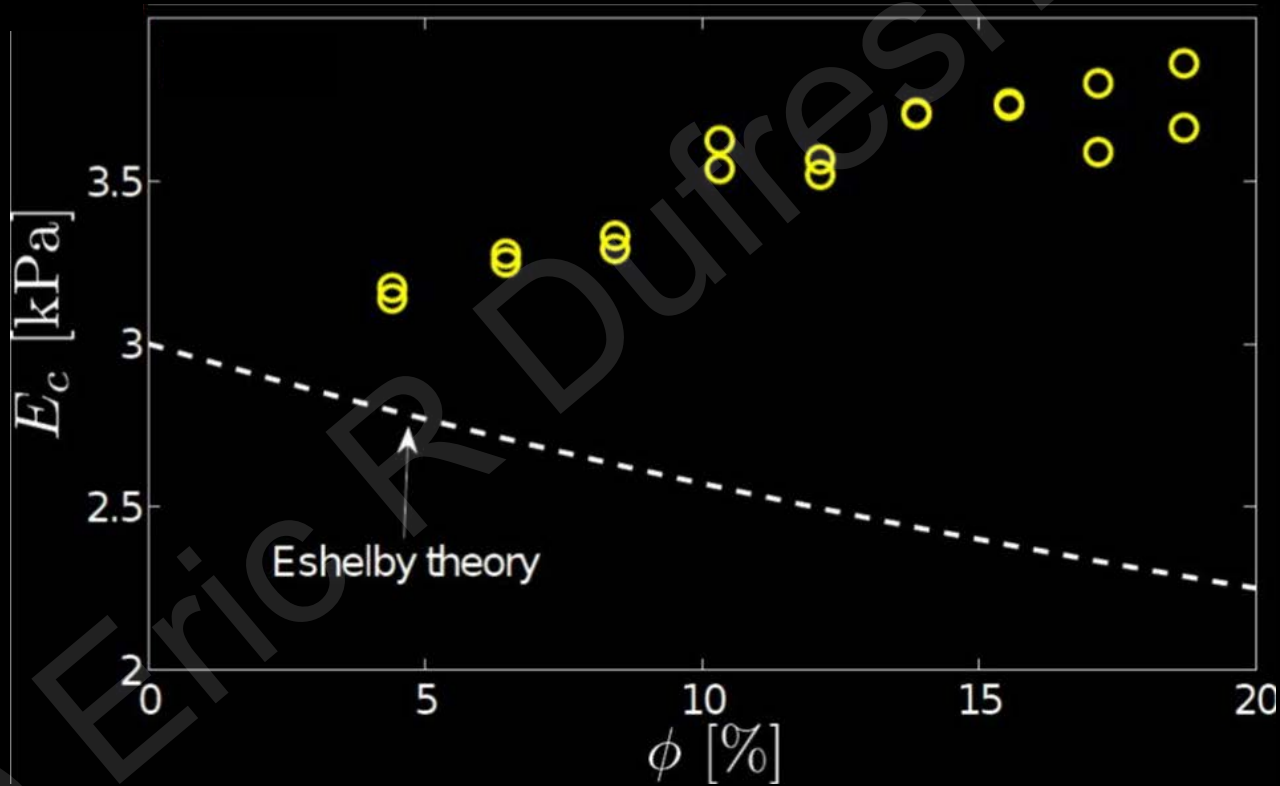
fluid

# Micron-scale glycerol droplets soften 100KPa PDMS

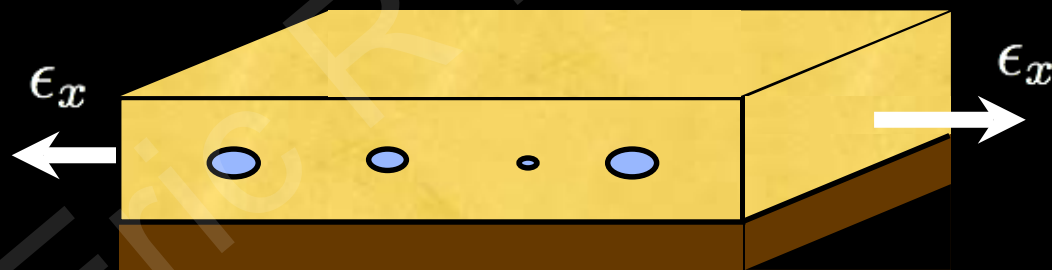
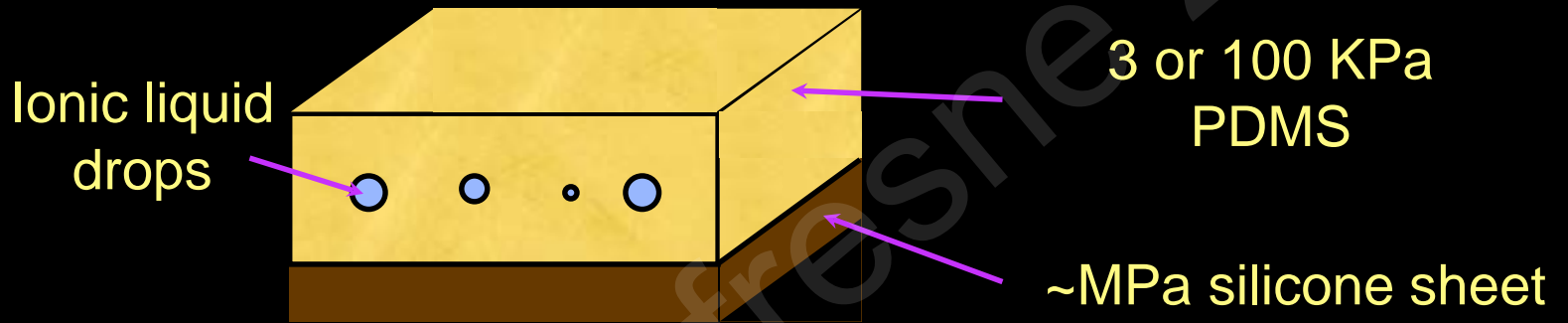


# Micron-scale glycerol droplets stiffen 3 KPa PDMS

➔ *Elastic theory works for stiff matrices, but not for soft!*

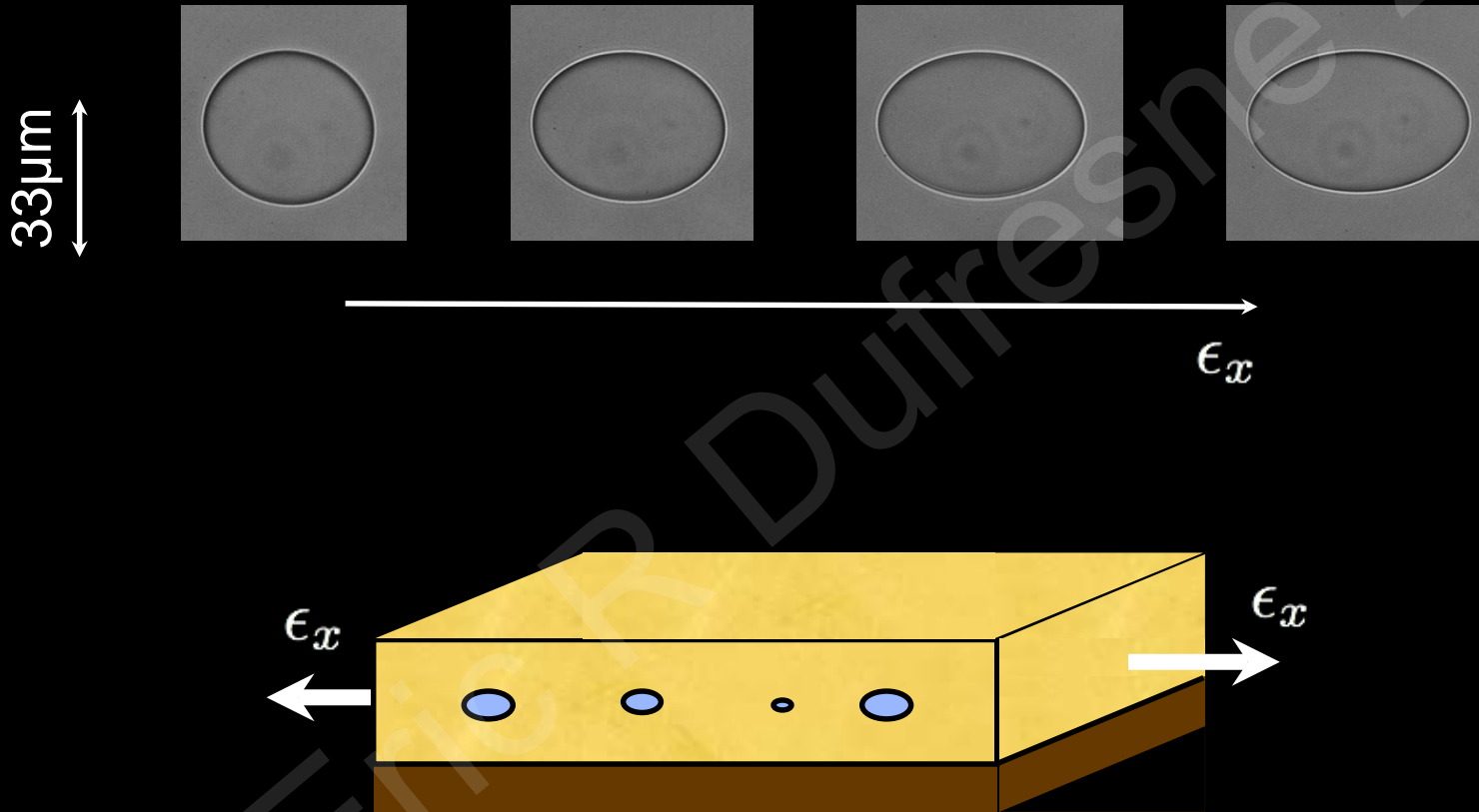


# Visualizing single inclusions

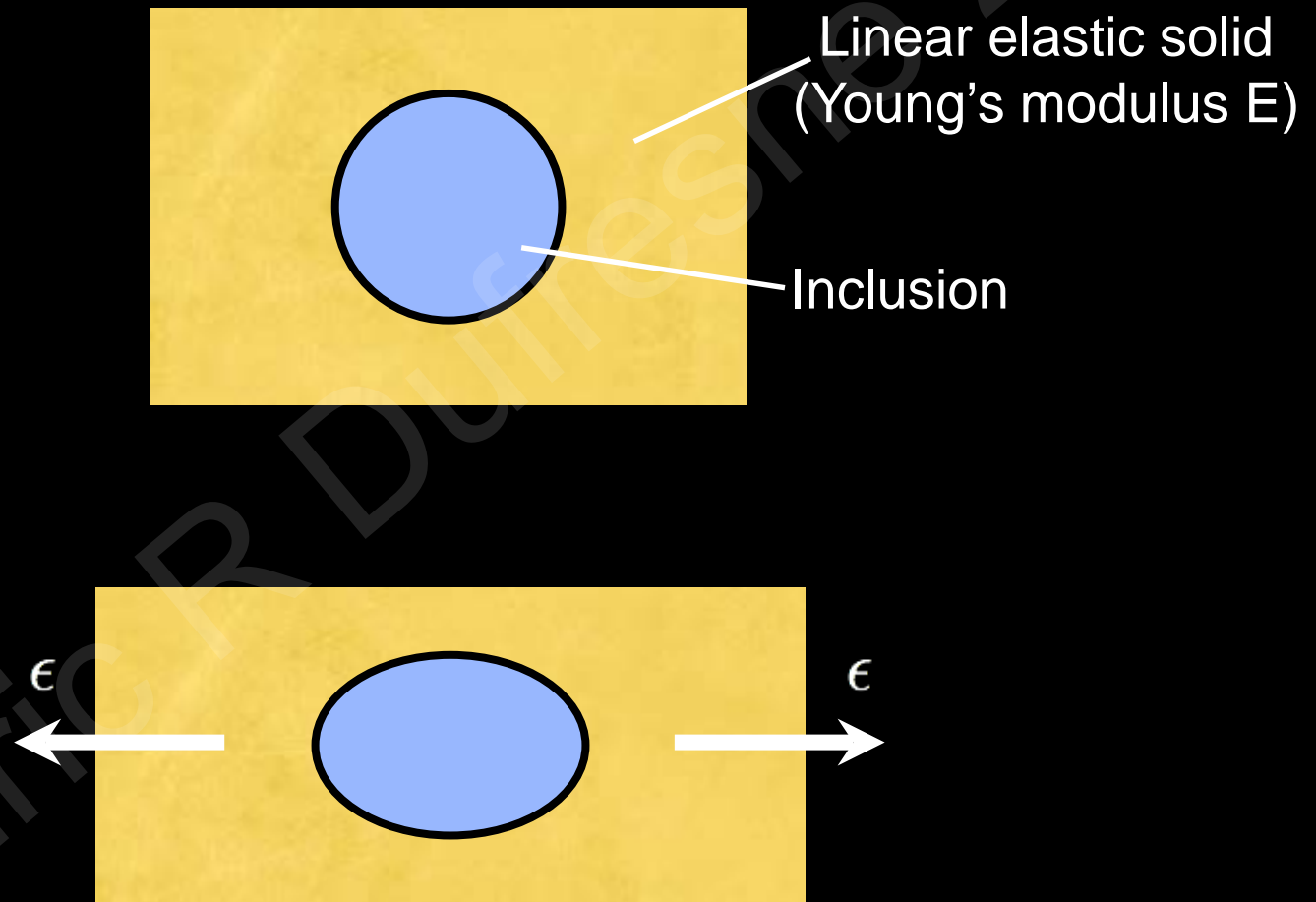




# Visualizing single inclusions

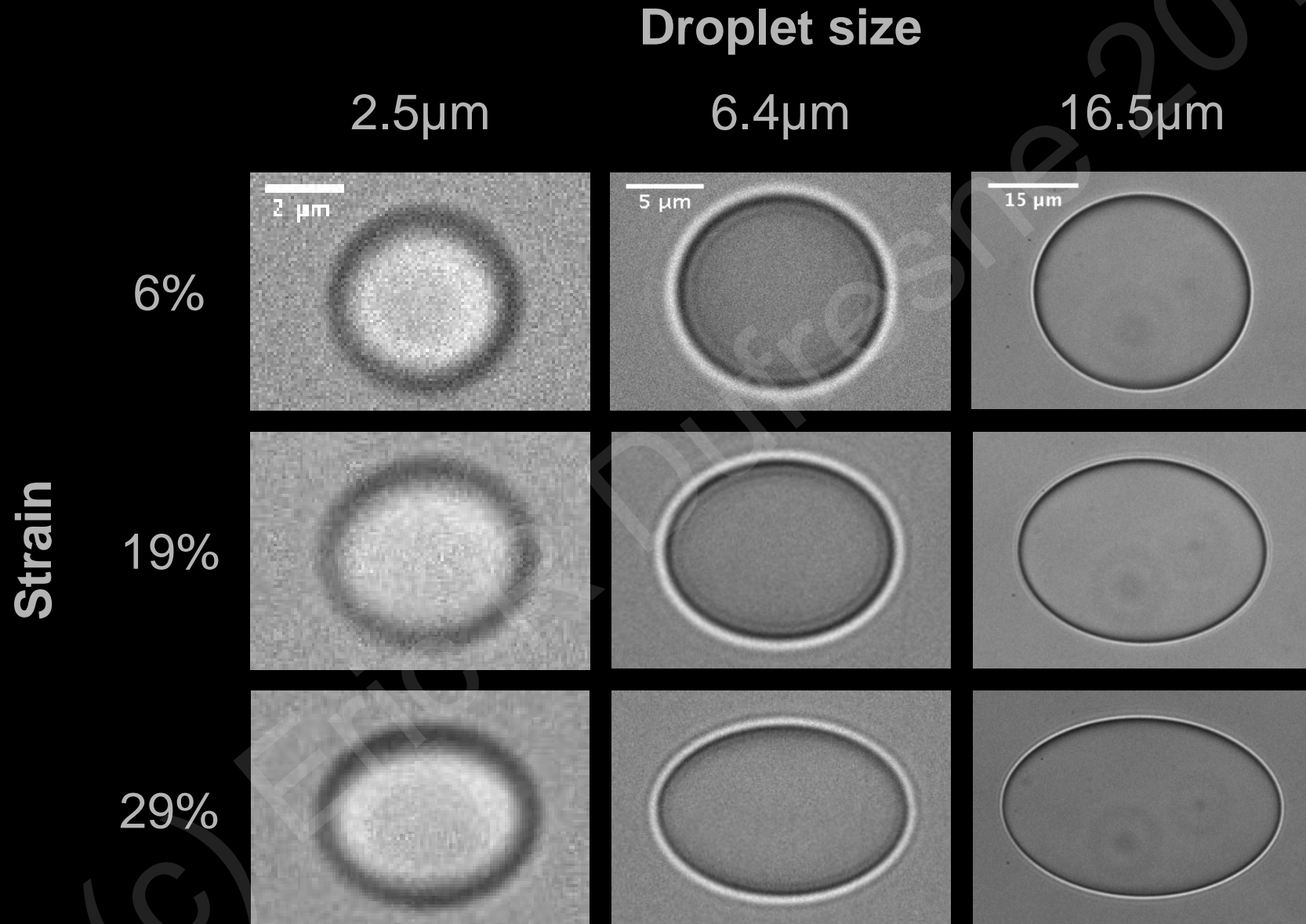


Elastic theory says drop shape should depend on strain...  
not size or stiffness

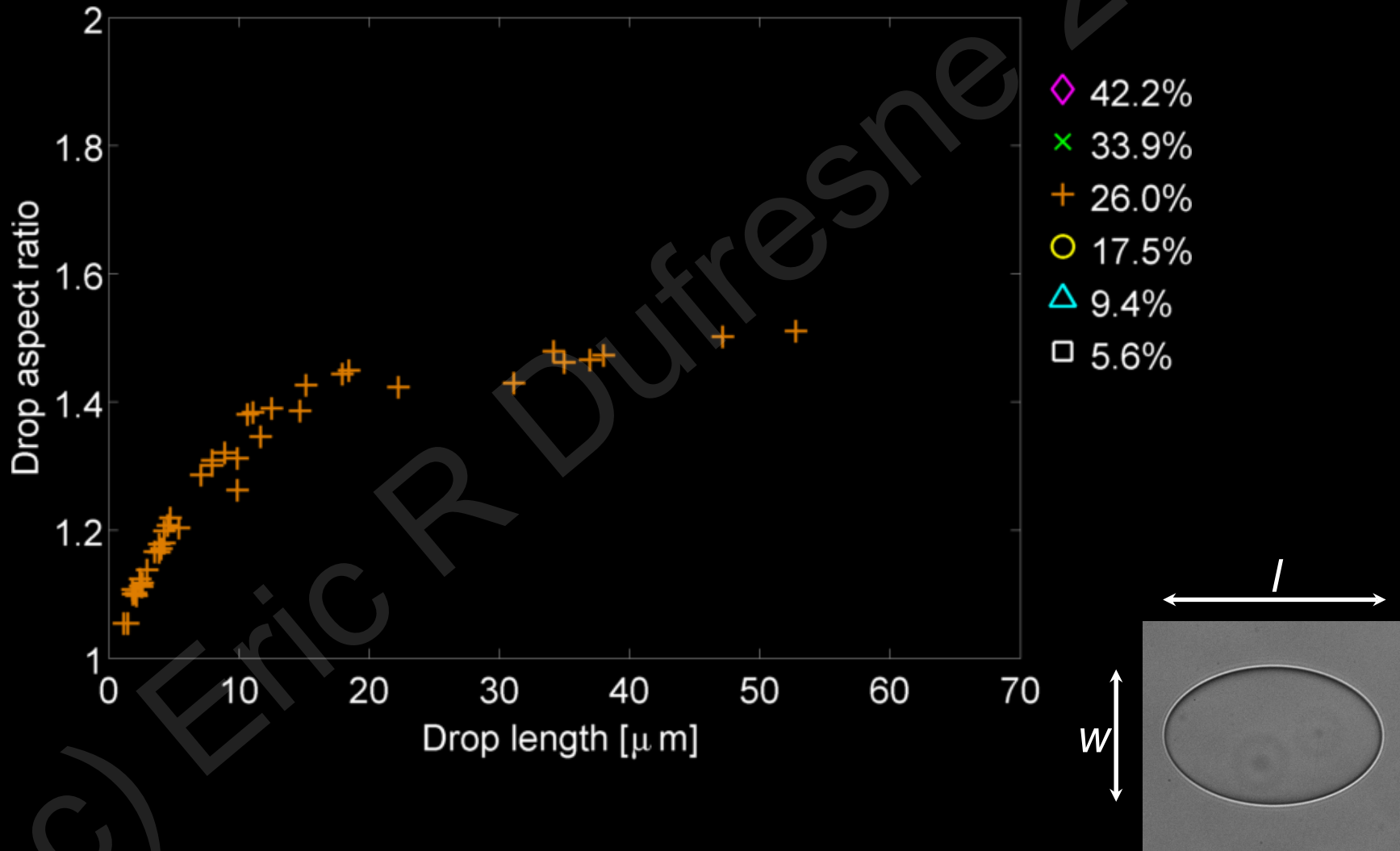


(Eshelby, 1957)

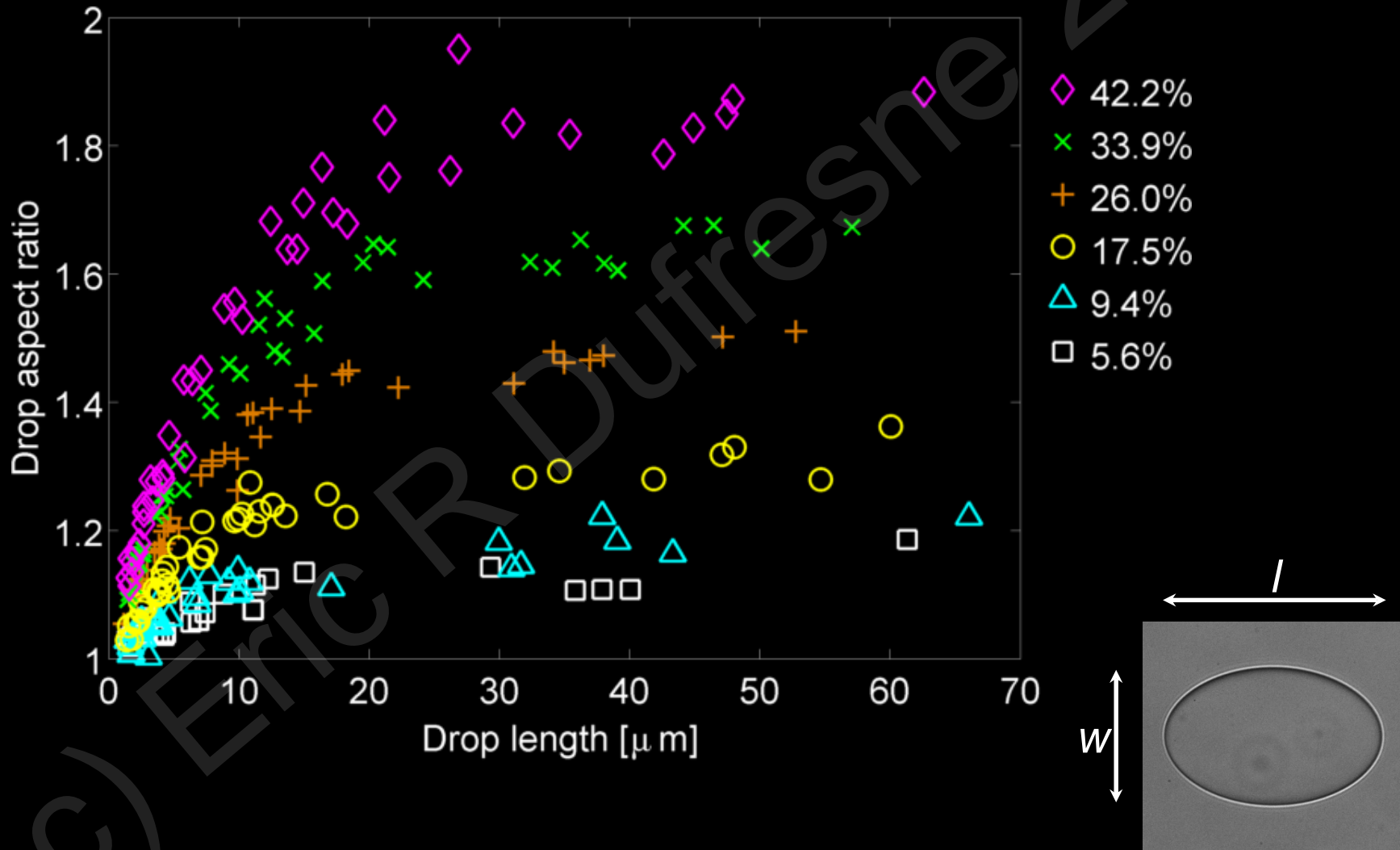
# Bigger droplets deform more than little ones



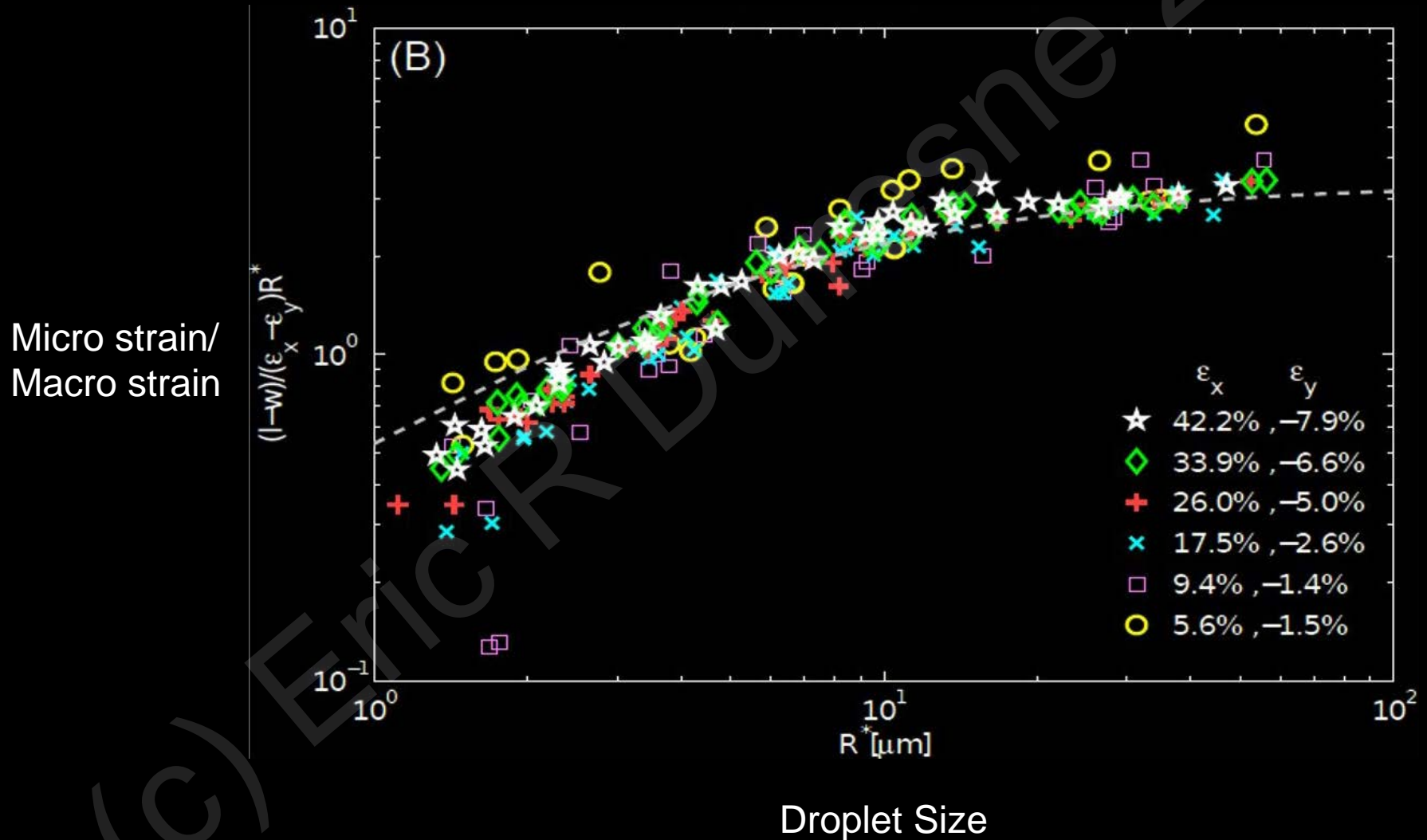
# Scale-dependent deformation



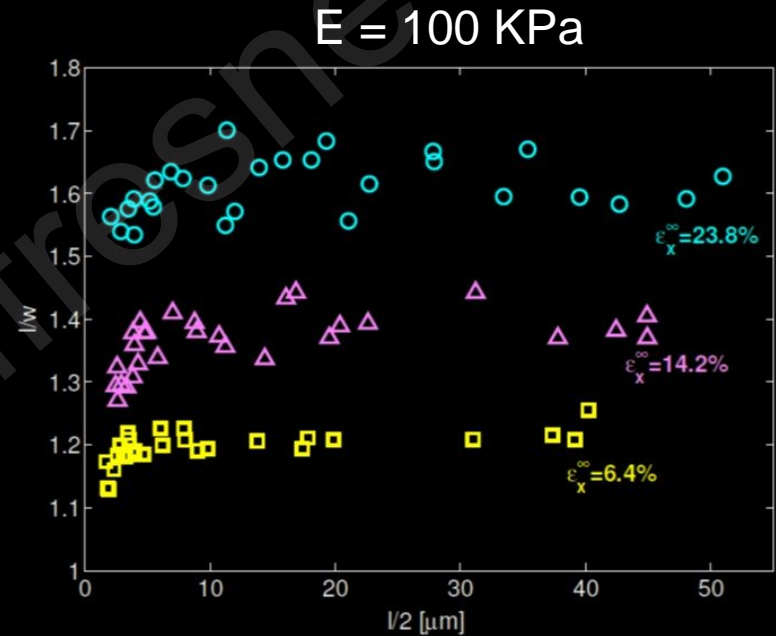
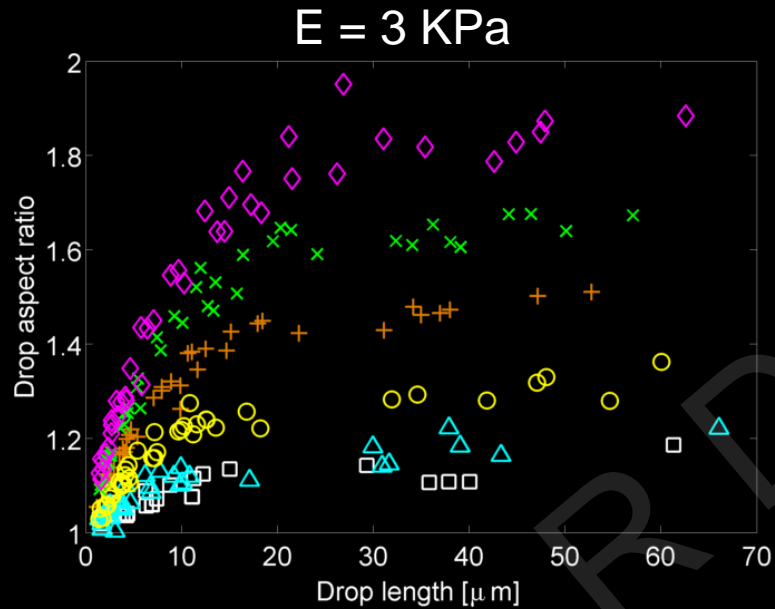
# Scale-dependent deformation



Far-field strain collapses droplet strain...  
...and a length scale emerges!

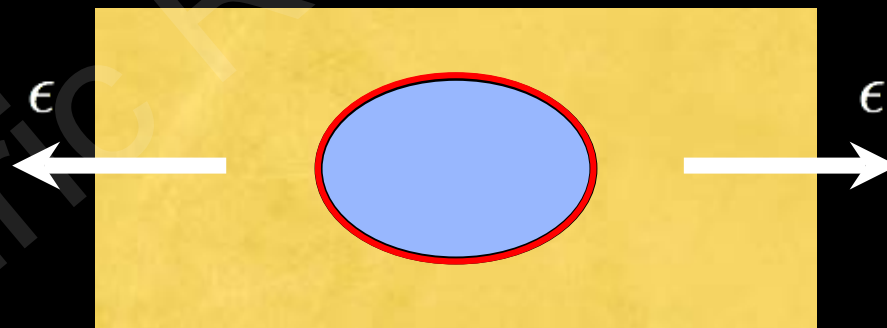
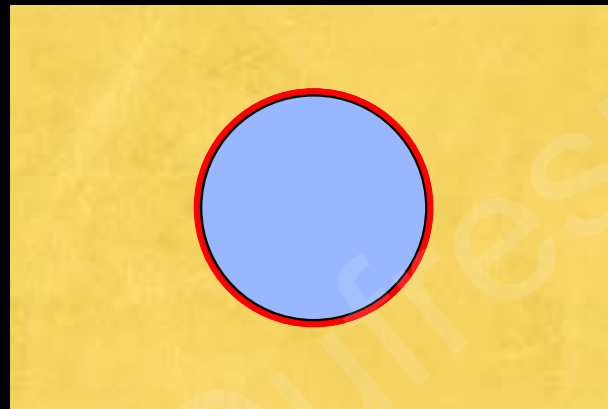


# Microscopic response depends on size and stiffness



Elastic theory says this response should be *independent* of size and stiffness

Classic elastic theories ignore the interface





More generally, surface tension creates a normal-stress jump across curved interfaces

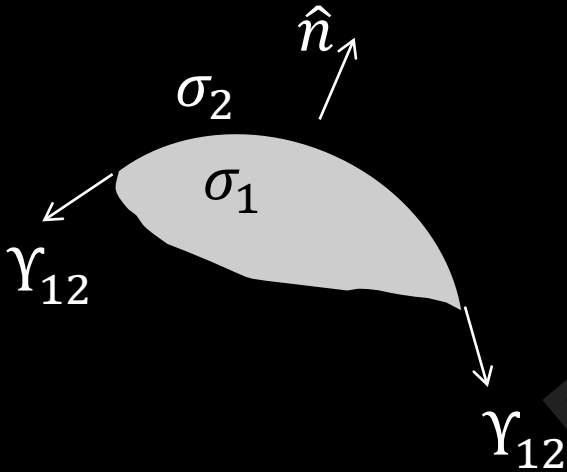
Generalized Young-Laplace:

$$(\sigma_2 - \sigma_1) \cdot \hat{n} = \gamma_{12} \kappa \hat{n}$$

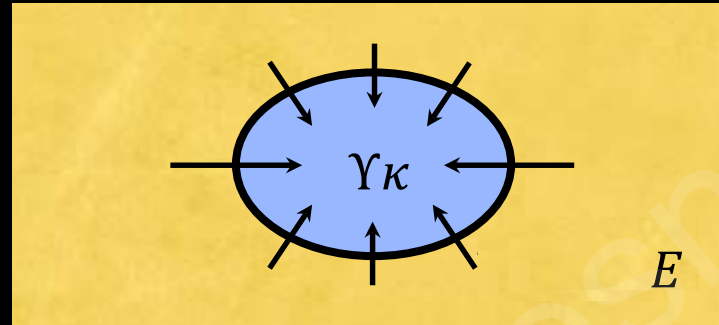
total curvature:  $\kappa = \partial_i n_i$

surface tension,  $\gamma_{12}$ :

*i.e.* surface stress assumed to be isotropic



# Surface tension can drive elastic deformation



$$\gamma\kappa \sim \varepsilon E$$

$$\varepsilon \sim \kappa \frac{\gamma}{E}$$

—  
material  
property

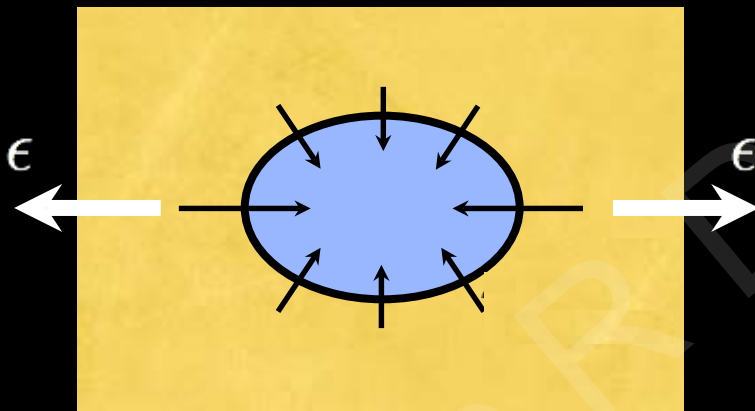
# Microscopic response to macroscopic strain

$$\kappa\gamma/E \ll 1$$

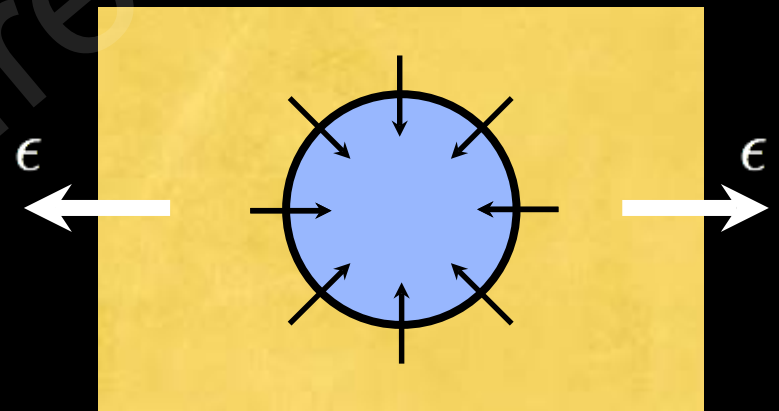
$$\gamma/ER \ll 1$$

$$\kappa\gamma/E \gg 1$$

$$\gamma/ER \gg 1$$



*bulk elasticity  
dominates*

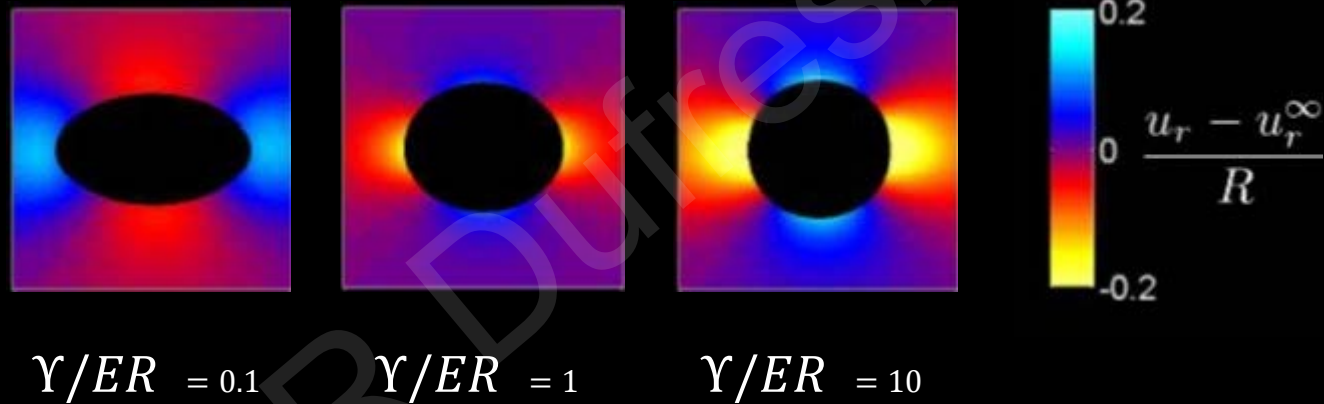


*surface tension  
dominates*

# Eshelby with Surface Tension (analytic)

*strain independent surface tension, no shear stress at the interface*

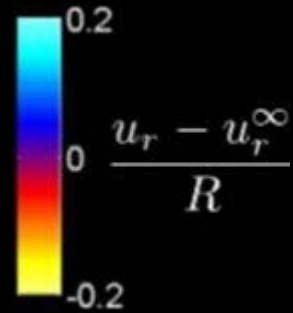
macroscopic strain 0.3



$\gamma/ER = 0.1$

$\gamma/ER = 1$

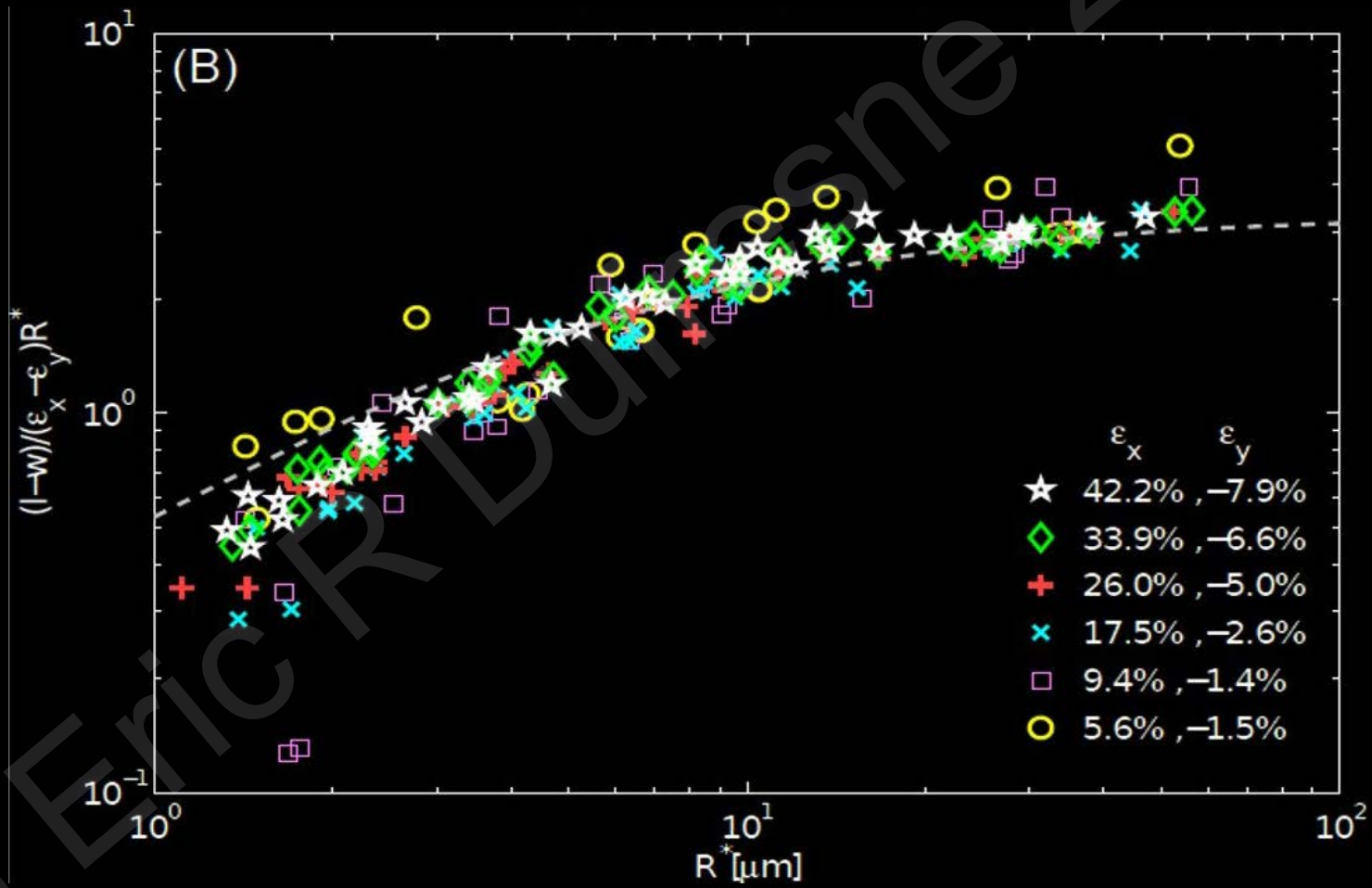
$\gamma/ER = 10$



Increasing surface tension

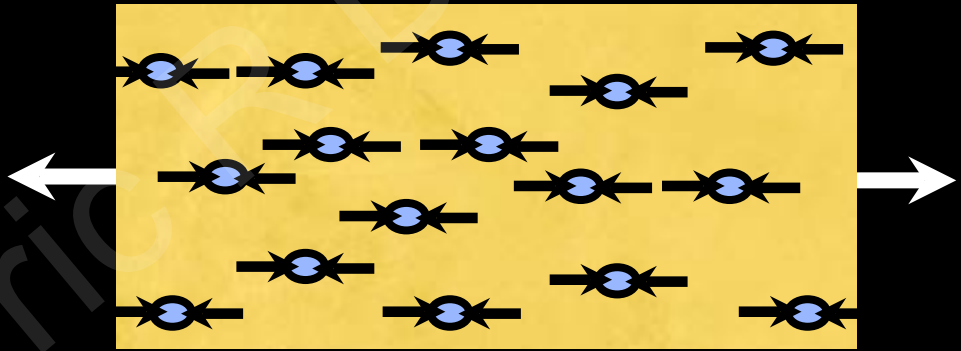
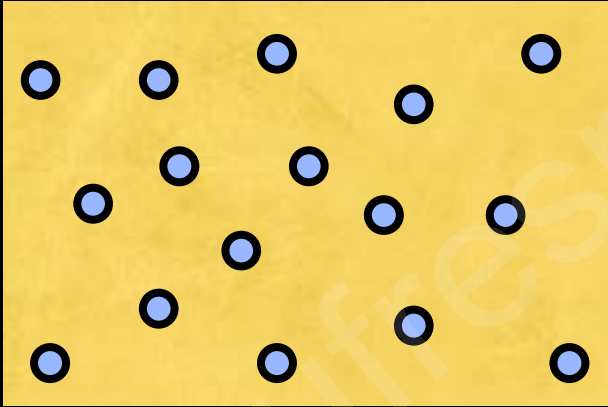
# Linear elastic theory with surface tension captures single droplet trend

Micro strain/  
Macro strain

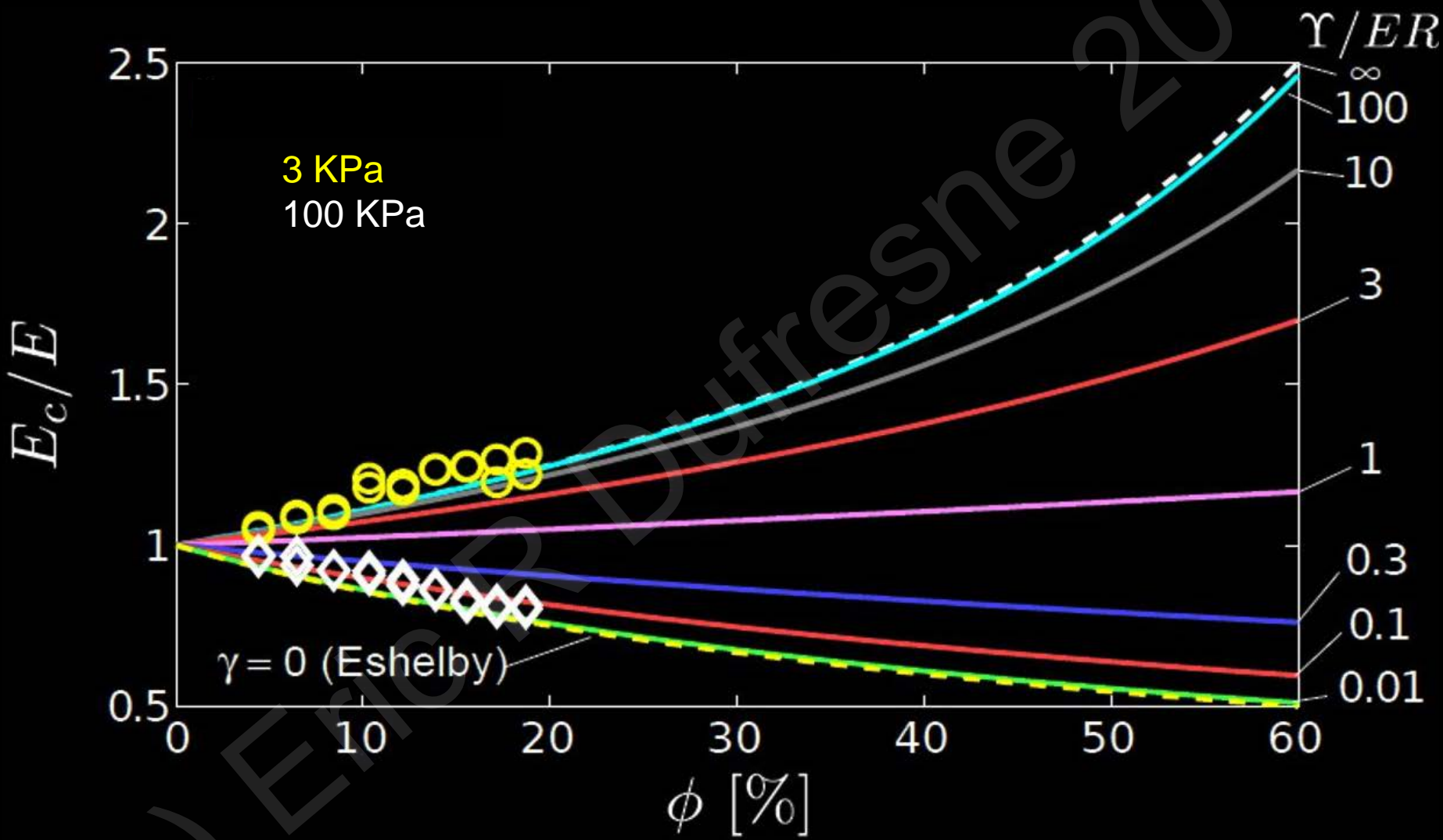


Droplet Size

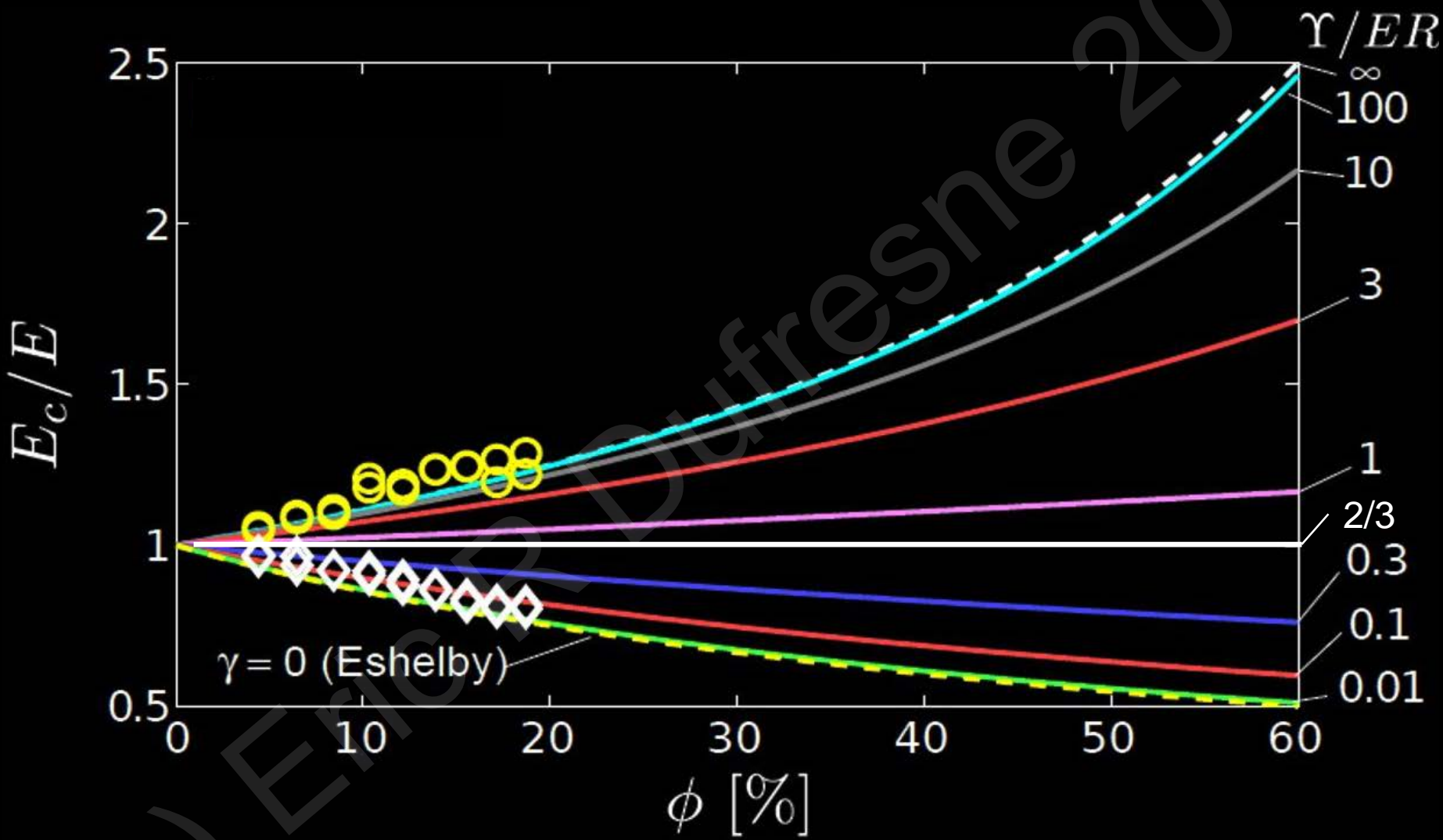
Surface tension 'pulls back' when the bulk solid attempts to deform embedded droplets



# Composite Stiffness Dilute Limit (Eshelby Method)



# Composite Stiffness Dilute Limit (Eshelby Method)





# Inclusions in Soft Solids

- When liquid inclusions are smaller than  $\Upsilon/E$ , surface tension dominates bulk elastic response
- In this limit, fluid inclusions *stiffen* soft solids
- Need to revisit applications of Eshelby, e.g. fracture mechanics
- More generally, surface tension dominates elastic response when  $\kappa\Upsilon/E \gg 1$
- References:
  - *Experiment*: Style et al Nature Physics 2015
  - *Theory*: Style et al Soft Matter 2015

# The Big Picture

Classic theories of solid mechanics fail when  $\kappa\Upsilon/E \gtrsim 1$



Soft solids can behave very differently than stiff ones.

Implications for cellular biomechanics...

Many solid mechanics problems need to be revisited...