

# Morphology of nematic and smectic vesicles

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Recent experiments on vesicles formed from block copolymers with liquid-crystalline side chains reveal a rich variety of vesicle morphologies. The additional internal order ("structure") developed by these self-assembled block copolymer vesicles can lead to significantly deformed vesicles as a result of the delicate interplay between two-dimensional ordering and vesicle shape. The inevitable topological defects in structured vesicles of spherical topology also play an essential role in controlling the final vesicle morphology. Here we develop a minimal theoretical model for the morphology of the membrane structure with internal nematic/smectic order. Using both analytic and numerical approaches, we show that the possible low free energy morphologies include nano-size cylindrical micelles (nano-fibers), faceted tetrahedral vesicles, and ellipsoidal vesicles, as well as cylindrical vesicles. The tetrahedral vesicle is a particularly fascinating example of a faceted liquid-crystalline membrane. Faceted liquid vesicles may lead to the design of supramolecular structures with tetrahedral symmetry and new classes of nano-carriers.

amphiphilic block copolymers | bending energy | Frank free energy | liquid crystalline polymers | self-assembled bilayer

Amphiphilic block copolymers in water, like natural phospholipids, can self-assemble into various monolayer or bilayer structures, such as micelles and vesicles (1, 2). In particular, rod-coil block copolymers, with a flexible hydrophilic chain and one or more rod-like hydrophobic blocks, exhibit a rich morphology of structures, and therefore have significant potential to advance fundamental science and drive technological innovations (3–12). Among these rod-coil block copolymers, we are especially interested in liquid crystalline (LC) block copolymers in which the hydrophobic block is a nematic or smectic liquid crystal polymer (13–20). The in-plane LC order that results from molecular pair interactions in these systems, and the associated defect structure, play very important roles in determining the preferred intermediate and final shapes of vesicles. The tailor-design of both material properties and vesicle morphology by controlling the molecular structures of the block polymers is state-of-the-art research in the fields of polymer science, materials science, and chemical engineering.

Some of the structures formed by these LC side-chain block copolymers in aqueous solution are rather counterintuitive, such as faceted vesicles, nanotubes and compact vesicles with tiny inner space (15, 20). In all these structures, the in-plane smectic order is clearly visible under Cryo-TEM. In this article we develop a theoretical explanation of the geometric structures of vesicles with in-plane nematic or smectic order. We present a simple model free energy as a functional of both the membrane geometry and the in-plane nematic order. Using both analytic and numerical methods, we then analyze the low free energy morphologies in various parameter regimes.

## Results and Discussions

Focusing on their overall shape we first perform a mean-field analysis of the model free energy of a self-assembled monolayer as a functional of their shape and nematic order parameters (21, 22):

$$H_m = \frac{1}{2} \int \sqrt{g} d^2x [K(\bar{D}\hat{n})^2 + \kappa(H - H_0)^2] \quad [1]$$

Here  $K$  is the Frank constant in the one-constant approximation, while  $\bar{D}$  denotes the covariant derivative.  $H$  is the mean curvature and  $H_0$  is the spontaneous curvature, which is determined by the asymmetry in the sizes of the hydrophobic and the hydrophilic parts of the LC block copolymers. We shall choose the normal vector of the monolayer to point from the hydrophobic side to the hydrophilic side. Therefore  $H > 0$  means that the hydrophilic side is bending outwards.

All three parameters  $K$ ,  $\kappa$ ,  $H_0$  depend on the chemical structures of the block copolymers as well as their interaction with the solvent in a complicated way. Furthermore, strictly speaking, a nematic membrane is locally anisotropic. Therefore its Frank free energy is characterized by two constants: one for splay ( $K_1$ ) and one for bend ( $K_3$ ). Likewise, the bending energy as well as the spontaneous curvature should also be generically anisotropic, characterized by three bending constants and three spontaneous curvature components. Such a model is characterized by eight independent parameters and is extremely complicated to analyze. For the sake of simplicity, we shall focus on the greatly simplified toy model Eq. 1, which captures the essential physics of nematic vesicles, which is the competition between the extrinsic bending energy and the two-dimensional Frank free energy.

A more important, conceptual issue is the following: In what sense can the vesicle morphology be understood in terms of minimization of elastic free energy Eq. 1? As is well known, the formation of vesicles is a complicated nonequilibrium process. Whether a certain property of a vesicle is distributed according to Gibbs-Boltzmann depends on the relevant experimental time scale, and on the time scale at which the given property equilibrates. At the stage of vesicle formation, individual molecules on the membrane can diffuse quite efficiently. Motion of liquid crystalline defects, however, requires coherent movement of all polymers on the vesicle, and is usually very slow. Hence we expect that the vesicle morphology achieves a local thermal equilibrium, where the shape and LC order minimizes the elastic free energy Eq. 1 (with appropriate parameters corresponding to the physical conditions under which the self-assembly takes place), subject to global constraints of given vesicle topology and LC defects distribution. We shall then enumerate all possible vesicle topologies and compare these free energy minima. It is interesting to note that in recent experiments by Jia et al. (13), multiple vesicle topologies were often observed using a given preparation method, sug-

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gesting that kinetics of self-assembly also played an important role in the selection of vesicle morphology.

Smectic vesicles can also be viewed as nematic vesicles with bending constant much larger than splay constant. On a membrane with in-plane smectic order, therefore, the bending deformation of the nematic director field should vanish everywhere. Mathematically this is equivalent to  $\hat{n} \cdot D\hat{n} = 0$ , that is, the nematic director locally follows the geodesics. This is always possible, for an arbitrary but prescribed membrane shape, except at the core of nematic disclinations. For these configurations, the Frank free energy becomes independent of the bending constant. Hence Eq. 1 is also a toy model for membranes with in-plane smectic order, with the understanding that  $K$  is the splay constant and the nematic director strictly follows the local geodesics.

Minimization of the Frank free energy in Eq. 1 requires that the covariant derivatives of the nematic director field vanish everywhere on the surface. As is well known in differential geometry, this is possible only if the Gaussian curvature vanishes everywhere; i.e. the surface is a *developable surface*. The family of developable surfaces includes planes, cylinders, cones, and tangent developable surfaces\*. On the other hand, minimization of the bending energy in Eq. 1 leads to a constant mean curvature  $H_0$ . It is clear that the only geometry minimizing both terms in the free energy in Eq. 1 is a cylindrical monolayer with a given radius  $1/H_0$ . In the recent example of Jia et al. (13), for example, where only aqueous solvent is present at the final stage of assembly, monolayer cylinders with very small radius (nano-fibers) are observed. The inner space of the cylinders is completely filled by the hydrophobic parts of the polymers. In order to form monolayer cylinders with larger radius, the inner space has to be filled by solvents (or other polymers) that are friendly to LC blocks. If there is only aqueous solvent, and if  $1/H_0$  is not small, monolayer cylindrical structures with favorable spontaneous curvatures cannot pack space and therefore the system should form certain kinds of bilayer structures, where two monolayers with opposite orientation stack together.

The free energy of a symmetric bilayer membrane can be obtained by adding up the free energies for two monolayers on both sides of the bilayer:

$$H_m = \int \sqrt{g} d^2x [K(\vec{D}\hat{n})^2 + \kappa H^2] \quad [2]$$

We shall focus on the morphology of symmetric bilayers in the remainder of this article. Note that area differences between the inner and outer layer can lead to nonvanishing spontaneous curvature (23, 24). These effects will not qualitatively change our conclusions.

Without considering the boundary effects, a flat bilayer with uniform nematic order clearly minimizes both terms in Eq. 2. The energy cost associated with the boundary, however, increases with the system size, and exceeds that associated with a closed vesicle with nonzero curvature, for sufficiently large systems (25). Closed vesicles therefore must form for sufficiently large bilayer membranes.

The morphology of a bilayer is controlled by the competition between the extrinsic bending energy and the Frank free energy. We shall first limit the discussion to closed vesicles of spherical topology. Since the total Gaussian curvature is nonvanishing, the system is frustrated and the Frank free energy competes with the bending energy. First consider the limiting case  $K \ll \kappa$ . The dominant contribution to the total energy is then the bending energy: minimizing this leads to a round spherical shape. For a more

realistic model where the bending energy is not isotropic, however, the shape will reflect the anisotropy of the bending moduli, leading to ellipsoidal shapes. The exact form of the shape as a function of the bending moduli is rather difficult to calculate, however, and will not be treated in this article. Ellipsoidal vesicles are frequently observed in the experiments of Jia et al. (14), with the smectic layers all perpendicular to the long axis of the ellipsoid. It can be inferred from this observation that the bending rigidity is higher along the nematic director than perpendicular to the director.

Let us now consider the opposite regime where  $K \gg \kappa$ . In this case, the system should first minimize the Frank free energy, which leads to developable surfaces with vanishing Gaussian curvature everywhere. This is clearly not possible due to Gauss' *Theorem Egregium*, which states that the total integrated Gaussian curvature of a surface with spherical topology is a topological invariant and equal to  $4\pi$ . There are faceted polyhedral surfaces, however, for which the Gaussian curvature vanishes everywhere but at a discrete number of (singular) vertices. These vertices are the ideal locations for orientational defects of the LC order (miserly loves company) (26). The total defect strength on a closed surface is also a topological invariant, according to the Gauss-Bonnet theorem. For nematic and smectic orders, this theorem dictates that on a sphere (or any other surface with the same topology), there are three possibilities for the structure of defects: (i) four disclinations each with strength  $+1/2$ ; (ii) two defects each with strength  $+1$ ; (iii) one strength  $+1$  defect and two strength  $+1/2$  defects. Now one needs at least four points to span a nondegenerate polyhedron; a tetrahedron in the minimal case. We conclude that in the limiting case  $K \gg \kappa$ , the ground state morphology of a vesicle with spherical topology is a faceted tetrahedron, with a strength  $1/2$  disclination located at each of the four corners. This structure is indeed observed in recent experiments (15, 20), as well as in our simulation, to be discussed in detail below. Note that the faceting observed here has a completely different origin to the well-known buckling of elastic shells where buckling occurs above a critical size  $R \sim \sqrt{\kappa/Y}$ , with  $Y$  the Young's modulus. The free energy Eq. 2, on the other hand, is scale free—the ground states are determined solely by the dimensionless ratio  $K/\kappa$ .

It is important to note that not all tetrahedra support a suitable nematic defect configuration. To ensure that the director field has vanishing covariant derivative everywhere except at the four vertices, but including the six edges, the sum of the three angles surrounding every vertex of the tetrahedron must be  $180^\circ$ . This imposes three constraints on the geometry of the tetrahedron†. Since the set of all tetrahedral shapes (up to scaling the overall size) forms a five-dimensional space, we see that the set of all fixed-size tetrahedra with vanishing covariant derivative everywhere except the vertices forms a *two-dimensional manifold*. Fig. 1 illustrates how these tetrahedra, together with a nematic director field with vanishing covariant derivative, can be constructed by folding a parallelogram. These tetrahedra have the special property that all four triangular facets are identical. All these structured smectic vesicles have vanishing Frank free energy. The degeneracy is lifted by different bending energies. The total free energy of the system is given by the sum of the bending energies localized on the six edges and the defect core energies localized at the four vertices. It is rather easy to see that for a given total surface area, the regular tetrahedron has a minimal value for the sum of all edge lengths. Thus the *ground state morphology of a smectic vesicle with spherical topology is a regular tetrahedron when the bending rigidity is vanishingly small*. The transition between different shapes is probably extremely slow, however, as it requires

\*Surfaces spanned by tangent lines of a spatial curve: a generic tangent developable surface that is topologically identical to plane is however not expected to be observed in experiments, because it can easily relax to a plane which has bending energy. It is not clear to us whether there exists a tangent developable surface that is topologically different from all the aforementioned structures.

†Naively we see there are four constraints but the condition for one vertex follows automatically from the constraints for the other three.



played in Fig. 2. For convenience we set  $K = 1$ . This does not change any essential physics since the vesicle morphology depends only on the dimensionless ratio  $\kappa/K$ . As the bending rigidity  $\kappa$  decreases, the vesicles with an isotropic Frank elastic constant undergo substantial shape deformation: (i) the almost spherical morphology is found to be stable at large  $\kappa$  (Fig. 2 *A* and *D*); (ii) ridges connecting four defects develop as  $\kappa$  becomes smaller than 1 (Fig. 2 *B* and *E*); (iii) a tetrahedral vesicle forms at a vanishingly small  $\kappa = 0.05$  (Fig. 2 *C* and *F*). The faceting transition occurs near  $\kappa \approx 1 \ddagger$ . The stable morphologies are determined by a delicate balance between the in-plane Frank energy and the bending energy as the surface deforms away from round. Indeed, as  $\kappa$  decreases from 100.0 to 0.05, the Frank free energy falls from 62.83 to 57.1 at the expense of bending energy which increases from 12.55 to 18.58. The Frank energy is localized near the four defects, which consequently induce deformation around the vertices. Our simulations are therefore entirely consistent with our prediction that spherical vesicles are stable in the regime of  $K \ll \kappa$ , whereas the faceted tetrahedral vesicles become stable in the other extreme  $K \gg \kappa$ .

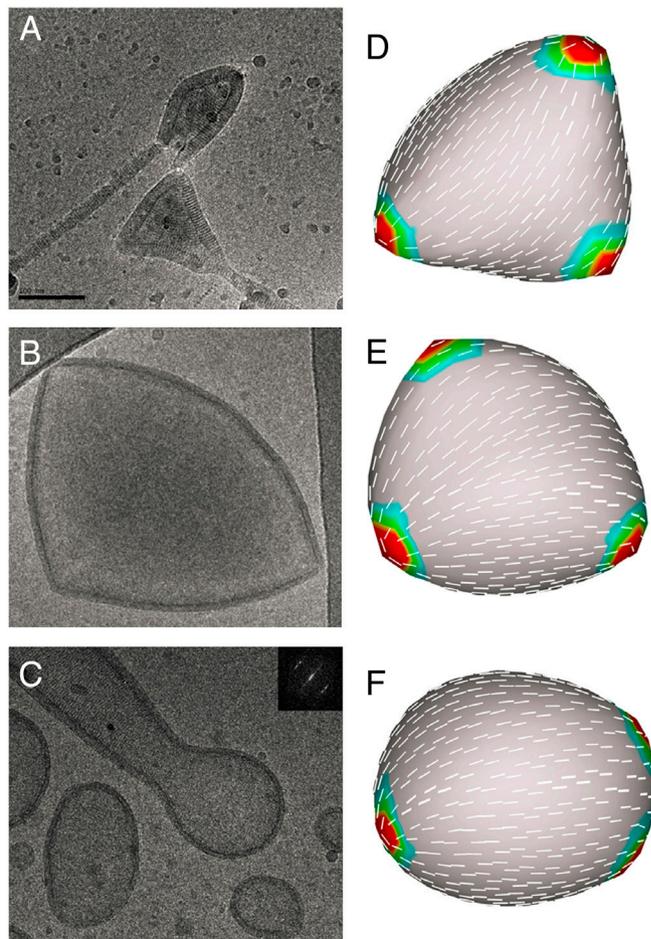
We also explore the effect of anisotropy in the Frank elastic constants by studying the regime in which splay dominates over bend. The smectic regime, as noted earlier, corresponds to the limit  $K_3 \gg K_1$ . In the current simulation, the anisotropy is estimated to be  $K_3/K_1 \approx 2.0$  (see *Supporting Information*). Although the shape transition trends are qualitatively similar for both the one-Frank constant and anisotropic cases, the anisotropy leads to a more dramatic shape transition, resulting in a considerably more faceted tetrahedral vesicle at a very small  $\kappa = 0.04$ , as displayed in Figs. 2 *G* and *H*. In fact, the splay dominant nematic texture enhances the faceting more than the isotropic case does. This is clearly understood by considering two membranes which possess a  $+1$  disclination defect with pure splay and pure bending nematic textures, respectively. The pure splay always decreases the Frank energy by buckling out-of-plane, because it allows the defect to escape into the third dimension and thus better align the nematic directors. On the other hand, such out-of-plane deformation of the pure bending does not alter the Frank energy and therefore, the faceting of pure bending membranes is not favorable upon deformation. Note that we are restricting ourselves here to the case of isotropic bending rigidity.

More prominent shape changes for vesicles with the anisotropic Frank elastic constants are clearly confirmed from a quantitative measurement of the asphericity (i.e., degree of deviation from the reference unit sphere geometry), which is defined as follows:

$$\frac{\langle \Delta R^2 \rangle}{R_{\text{ref}}^2} = \frac{1}{N} \sum_{\alpha=1}^N \frac{(R_{\alpha} - R_{\text{ref}})^2}{R_{\text{ref}}^2}, \quad [5]$$

where  $R_{\alpha}$  is the radial distance of vertex  $\alpha$ ,  $R_{\text{ref}}$  is the radius of the reference unit sphere, and  $N$  is the total number of vertices. The asphericities are averaged over 10 simulation runs for each  $\kappa$  and plotted in Fig. 2 as a function of  $1/\kappa$ . The plot exhibits relatively large deviations from its average values, especially at low bending rigidity. This is mainly attributable to the differences in the asphericity between the three possible ground state morphologies. Although faceted tetrahedral vesicles are expected to be the ground state for large system sizes, we have observed in our simulation three different ground state morphologies, presumably due to its finite system size: (i) an ellipsoidal vesicle with two closely bounded disclination pairs; (ii) a flattened (square cushion-shape) vesicle with four  $+1/2$  disclinations located approximately in one plane; and (iii) a tetrahedral vesicle with four well separated  $+1/2$  defects (see *Supporting Information*). These three morphologies

<sup>†</sup>We emphasize, however, that these morphological changes are smooth crossovers. There is no real phase transition in the thermodynamic sense.



**Fig. 3.** Comparison between experimental observations (A)–(C) and computer simulations (D)–(F). *Left:* Experimental results, (A) a tetrahedral smectic vesicle (20); (B) a fat tetrahedral smectic vesicle (15); (C) an ellipsoidal smectic vesicle (14). *Right:* Simulation results for a case of  $K_3/K_1 \approx 2.0$ , (D)  $\kappa = 0.04$ ; (E)  $\kappa = 0.1$ ; (F)  $\kappa = 0.5$ . The contour plots show the distribution of the local Frank free energy.

seem degenerate as the differences in their total free energies are within 0.5%. These vesicle shapes can be viewed as the precursors of the extreme morphologies at  $\kappa \rightarrow 0$ , such as long fibrous cylinders, double layer sheets, and sharply faceted tetrahedrons, respectively. Finally, we briefly compare our simulation results with our recent experimental observations in Fig. 3.

Complex shape phase diagrams are also possible for fluid vesicles with fixed internal volume (30). A feature of these morphologies is their nonconvex shape. Such nonconvexity has not been seen experimentally in the block copolymer systems studied here, leading us to believe that during the formation process solvent can freely enter and leave the system so that the internal volume is not conserved.

In conclusion, we have studied the fascinating morphology of nematic/smectic vesicles, such as the faceted tetrahedron, nanofibers, and ellipsoids using a simple toy model free energy $\S$ . Our theoretical and numerical studies provide the fundamental understanding of formation of these novel structured vesicles and elucidate the shape-selective mechanisms. It could also pave the way for formulating guiding principles in designing nanocarriers with specific shapes, particularly utilizing the two-dimensional nematic order and the topological defects, which are ubiquitous in closed vesicles.

<sup>§</sup>We note that other more complicated shapes may arise if we consider a more general model free energy where both bending rigidities and Frank constants are anisotropic.

## Methods

To implement a deformable lattice model with spherical topology, we first introduce a reference sphere and tessellate it with a triangular mesh along with 12 requisite 5-disclinations. Afterward a dual lattice of the triangular mesh is constructed, each dual site being the center of mass of each plaquette formed by the original triangular lattice. The details of the lattice geometry are illustrated in the *Supporting Information*. Let  $\hat{m}_\alpha$  to be the unit vector normal to the plaquette  $\alpha$ . A director  $\hat{n}_\alpha$  and a projection operator  $\hat{N}_\alpha = \hat{n}_\alpha \hat{n}_\alpha$  are defined on each dual site with a constraint that it must be perpendicular to the plaquette normal:  $\hat{N}_\alpha \cdot \hat{m}_\alpha = 0$ .

Let  $d_{\alpha\beta}$  be the bond length connecting two neighboring dual sites  $\alpha$  and  $\beta$ , and  $S_{\alpha\beta}$  be the area spanned by the bond  $\alpha\beta$ . The discretized Frank free energy is then given by

$$F_{\text{Frank}} = K \sum_{(\alpha\beta)} S_{\alpha\beta} d_{\alpha\beta}^{-2} \text{Tr}[(\hat{N}_\beta - \hat{N}_\alpha)^2] \quad [6]$$

The bond lengths  $d_{\alpha\beta}$  and the areas  $S_{\alpha\beta}$  are introduced to ensure that the lattice model is a proper discretization of the continuum model Eq. 2. They insure that, up to errors which scale with the plaquette area  $S_{\alpha\beta}$ , the lattice free energy is invariant under change of triangulation. The discrete reparametrization invariance is necessary so that the free energy depends only on vesicle shape and not on the specific structure of the mesh. This is implemented for each shape as the vertices are deformed.

The discretized bending energy is given by

$$F_{\text{bending}} = \kappa \sum_{\alpha} S_{\alpha} \text{Tr} \mathbf{K}_{\alpha}^2, \quad [7]$$

where  $\mathbf{K}_{\alpha}$  is the extrinsic curvature tensor at site  $\alpha$ , whilst  $S_{\alpha}$  is the area of the plaquette  $\alpha$ . The curvature tensor  $\mathbf{K}_{\alpha}$  of each plaquette  $\alpha$  can be calculated from the following three equations:

$$\begin{aligned} e_{\alpha\beta}^{\parallel} &= \frac{1}{2} \vec{e}_{\alpha\beta}^{\perp} \cdot \mathbf{K}_{\alpha} \cdot \vec{e}_{\alpha\beta}^{\perp} & e_{\alpha\gamma}^{\parallel} &= \frac{1}{2} \vec{e}_{\alpha\gamma}^{\perp} \cdot \mathbf{K}_{\alpha} \cdot \vec{e}_{\alpha\gamma}^{\perp} \\ e_{\alpha\delta}^{\parallel} &= \frac{1}{2} \vec{e}_{\alpha\delta}^{\perp} \cdot \mathbf{K}_{\alpha} \cdot \vec{e}_{\alpha\delta}^{\perp}, \end{aligned} \quad [8]$$

where  $\vec{e}_{\alpha\beta}$  is the vector pointing from vertex  $\alpha$  to vertex  $\beta$ , and  $e_{\alpha\beta}^{\parallel}$  and  $e_{\alpha\beta}^{\perp}$  are its components parallel and perpendicular to the plaquette normal  $\hat{m}_\alpha$ .

In the MC simulations, the deformable surface consists of 300 vertices, corresponding to 596 directors in all. The initial shape of the surface is a unit sphere and the initial director orientations are random. Each MC sweep consists of trial attempts to rotate each director and to move each vertex. The acceptance or rejection of a MC trial is determined by the standard Metropolis algorithm. All vertices are allowed to move along the radial direction with the angular positions of the vertices fixed. In order to preserve the total area upon surface deformation, any vertex moves making a total area change larger than 1% are rejected. Finally, once the surface is deformed by vertex moves, the orientations of directors are corrected by projecting them onto the newly deformed plaquette before the new free energy is calculated.

Finally we remark that we have checked carefully that the location of nematic defects is not influenced by the inevitable lattice disclinations associated with spherical topology and present in our meshes as described above.

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# Supporting Information

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## SI Text

Here we present the additional information of (i) the detailed description of the lattice geometry employed in our simulations, (ii) estimation of the splay ( $K_1$ ) and bending ( $K_3$ ) elastic constants, and (iii) simulation observations presenting three classes of degenerate morphologies in the lowest energy states.

**I. Dual Honeycomb Lattice.** During the course of our simulations, we use the dual honeycomb lattice, which is constructed from a triangular mesh on a sphere. In Fig. 1, we illustrate the lattice geometry. The dual honeycomb lattice sites are labeled by Greek letters and directors are defined on every dual lattice site. The two-body interaction can be calculated between neighboring directors, such as  $\alpha, \beta$ , etc., and three body interaction involves next-nearest neighbor triplet  $\alpha, \beta, \gamma$ , etc. The extrinsic curvature tensor  $\mathbf{K}_\alpha$  can be calculated at every dual lattice  $\alpha$ , as discussed in the main text.

**II. Estimation of the Splay ( $K_1$ ) and Bending ( $K_3$ ) Elastic Constants.** In addition to the isotropic case, where the Frank free energy is described in one constant limit  $K$  as shown in eq. 6 in the main text, we also studied the anisotropic case, where the splay and bending elastic constants are different; i.e.,  $K_1 \neq K_3$ . The anisotropy in the Frank elastic constants can be turned on if we include three body interactions as following,

$$F_{\text{Frank}} = J_2 \sum_{\langle \alpha\beta \rangle} S_{\alpha\beta} d_{\alpha\beta}^{-2} \text{Tr}[(\hat{N}_\beta - \hat{N}_\alpha)^2] + J_3 \sum_{\langle \alpha\beta\gamma \rangle} \sqrt{S_{\alpha\beta} S_{\alpha\gamma}} d_{\alpha\beta}^{-1} d_{\alpha\gamma}^{-1} (\hat{e}_{\alpha\beta} \cdot \hat{N}_\alpha \cdot \hat{e}_{\alpha\gamma}) \text{Tr}[(\hat{N}_\alpha - \hat{N}_\beta)(\hat{N}_\alpha - \hat{N}_\gamma)]. \quad [\text{S1}]$$

However, in our discretized model above, the relation between parameters such as, ( $J_2, J_3$ ) and the Frank elastic constants ( $K_1, K_3$ ) is not obvious, and also depends on the type of lattice geometry. Here we estimate  $K_1$  and  $K_3$  values, by comparing numerically calculated energy for given  $J_2$  and  $J_3$  from eq. 1 to the analytic Frank energy calculation in a flat space. We first prepare a large rectangular system with given lattice type (honeycomb lattice for our case), and apply a twisted boundary condition, in which the nematic directors at two opposite edges make a small angle difference  $\Delta\theta$  as shown in Fig. 2. The pure splay texture can be obtained by free energy minimization with the boundary condition as presented in the left in Fig. 2 and be used to determine  $K_1$ , while  $K_3$  can be estimated from the boundary condition as shown in the right in Fig. 2. The numerically minimized free energy cost of eq. 1 is then compared with the following analytic calculation:

$$\Delta F = \frac{K_i}{2} \int d^2x (\partial_x \theta)^2 = \frac{K_i H(\Delta\theta)^2}{2L}. \quad [\text{S2}]$$

The estimated anisotropy of  $K_3/K_1$  in the honeycomb lattice is found to be approximately 2.

**III. Three Representative Ground State Morphologies.** In Fig. 3, we illustrate three degenerate morphologies at a very small bending rigidity, which are found in our simulation at finite system size. The differences in the total free energies are within  $\pm 0.5\%$ . Such degeneracy is observed both in isotropic and anisotropic cases.

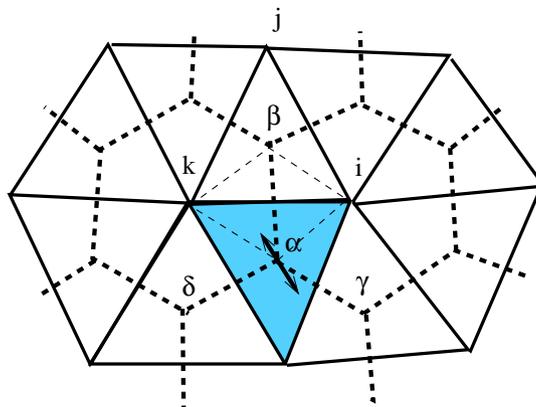
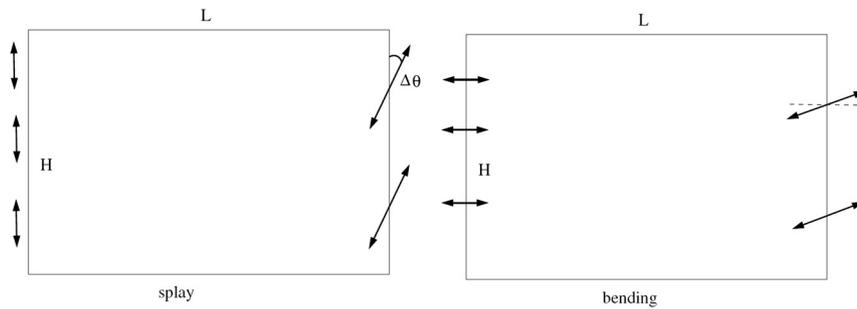
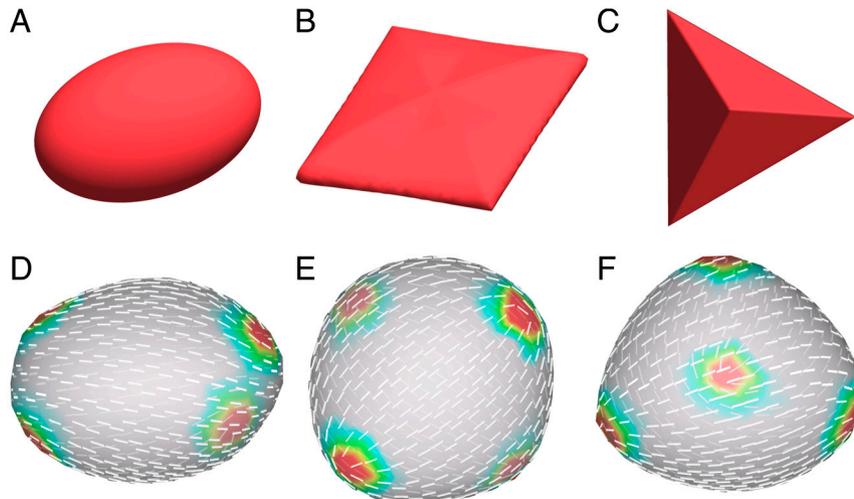


Fig. S1. A lattice geometry used in our simulations. Roman letters represent the lattice sites in the original triangular mesh, while Greek letters indicate the dual honeycomb lattice sites. The arrow on the lattice site  $\alpha$  represents a nematic director.



**Fig. S2.** How to numerically measure Frank constants  $K_1$  and  $K_3$  using spin wave method. Take a rectangular system and apply twisted boundary conditions on two opposite sides. The twist angle should be small enough. *Left:* splay constant. *Right:* bending constant.



**Fig. S3.** Three representative ground state morphologies. (A)–(C) show the schematic representation of three degenerate morphologies obtained from simulations in (D)–(F); (A) and (D), an ellipsoidal shape vesicle with two closely bounded disclination pairs; (B) and (E), a flattened vesicle with four well separated half integer disclinations located in one plane; (C) and (F), a tetrahedral vesicle with four well separated half integer disclinations. All simulation results are at  $\kappa = 0.05$  and for the case of  $K_1 = K_3$ .